

### DESCRIPTION

The MP2462 is a synchronous, step-down, switching regulator with integrated, internal, high-side and low-side power MOSFETs (HS-FETs and LS-FETs, respectively). It provides 2A of highly efficient output current ( $I_{OUT}$ ) with current-mode control for fast loop response.

The wide 4.2V to 32V input voltage ( $V_{IN}$ ) range accommodates a variety of step-down applications. A low shutdown-mode quiescent current allows the MP2462 to be used in battery-powered applications.

High power conversion efficiency across a wide load range is achieved by scaling down the switching frequency ( $f_{SW}$ ) under light-load conditions to reduce switching and gate driving losses.

Frequency foldback helps prevent inductor current ( $I_L$ ) runaway during start-up. Thermal shutdown provides reliable and fault-tolerant operation. A high duty cycle and low-dropout (LDO) mode are provided for battery-powered systems.

The MP2462 requires a minimal number of readily available, standard external components, and is available in a space-saving TSOT23-6 package.

### FEATURES

- Wide 4.2V to 32V Operating Input Voltage ( $V_{IN}$ ) Range
- 2A Continuous Output Current ( $I_{OUT}$ )
- 55 $\mu$ A Sleep-Mode Quiescent Current
- 160m $\Omega$ /80m $\Omega$  High-Side/Low-Side On Resistance ( $R_{DS(ON)}$ ) for Internal Power MOSFETs
- High Feedback (FB) Accuracy:  $\pm 0.7\%$  at  $T_J = 25^\circ\text{C}$ , or  $\pm 1\%$  at  $T_J = -40^\circ\text{C}$  to  $+125^\circ\text{C}$
- Internal Soft Start (SS)
- Fixed 800kHz Switching Frequency ( $f_{SW}$ )
- Low-Dropout (LDO) Mode
- Output Discharge
- Thermal Shutdown
- Over-Current Protection (OCP) with Hiccup Mode
- Available in a TSOT23-6 Package



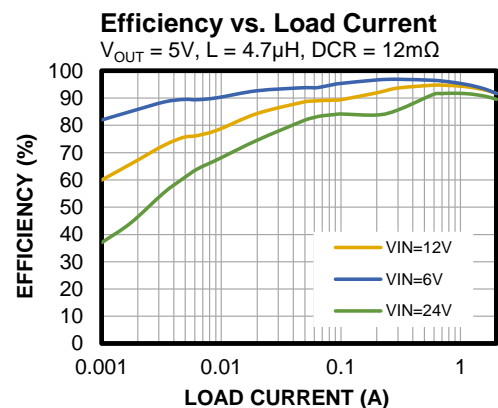
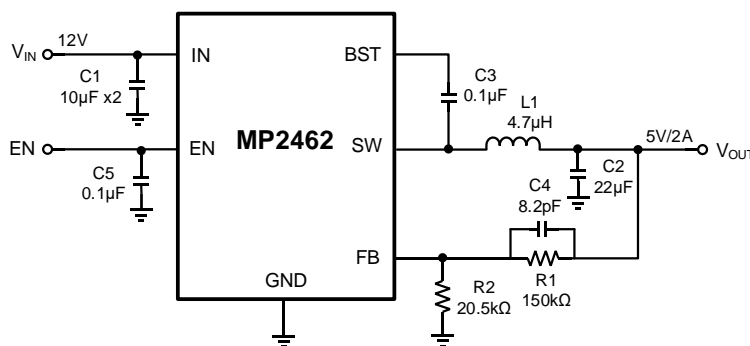
Optimized Performance with  
MPS Inductor MPL-AL6060 Series

### APPLICATIONS

- Battery-Powered Systems
- Smart Homes
- Wide Input Range Power Supplies
- Standby Power Supplies

All MPS parts are lead-free, halogen-free, and adhere to the RoHS directive. For MPS green status, please visit the MPS website under Quality Assurance. "MPS", the MPS logo, and "Simple, Easy Solutions" are trademarks of Monolithic Power Systems, Inc. or its subsidiaries.

### TYPICAL APPLICATION



### ORDERING INFORMATION

Part Number*	Package	Top Marking	MSL Rating
MP2462GJ	TSOT23-6	See Below	1

\* For Tape & Reel, add suffix -Z (e.g. MP2462GJ-Z).

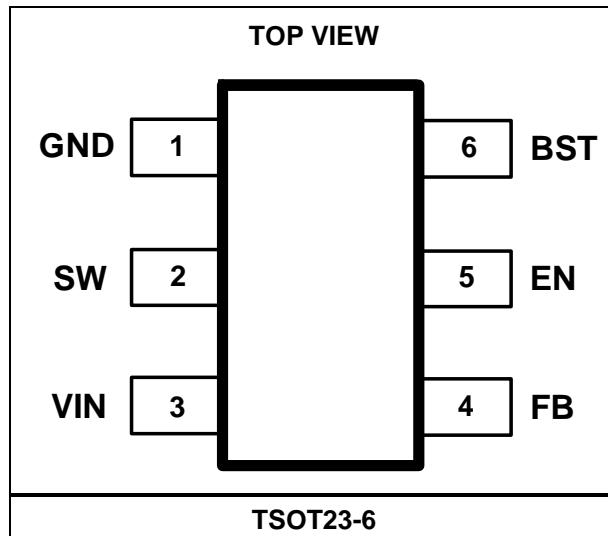
### TOP MARKING

**| BTDY**

BTD: Product code of MP2462GJ

Y: Year code

### PACKAGE REFERENCE



**PIN FUNCTIONS**

Pin #	Name	Description
1	GND	<b>System ground.</b> The GND pin is the reference ground of the regulated output voltage ( $V_{OUT}$ ), and requires extra care during PCB layout. Make the GND pin connections using copper traces and vias.
2	SW	<b>Switch output.</b> Make the SW pin connections using a wide PCB trace.
3	VIN	<b>Supply voltage.</b> The MP2462 operates from a 4.2V to 32V input rail. The VIN pin must be connected to a capacitor using a wide PCB trace to decouple the input rail.
4	FB	<b>Feedback.</b> Connect the FB pin to the tap of an external resistor divider connected between the output and GND to set $V_{OUT}$ . Place the resistor divider as close to FB as possible. Avoid vias on the FB traces and keep the trace far away from the SW node.
5	EN	<b>Enable.</b> The EN pin is a digital input that turns the buck regulator on or off. When the control circuit's power supply is ready, pull EN high to turn the buck regulator on; pull EN low to turn the regulator off. Connect EN to VIN via a voltage resistor divider for automatic start-up. Ensure that the EN pin voltage ( $V_{EN}$ ) does not exceed 5.5V.
6	BST	<b>Bootstrap.</b> Connect a capacitor between the BST and SW pins to form a floating supply across the high-side MOSFET (HS-FET) driver. It is typically recommended to use a 0.1 $\mu$ F BST capacitor ( $C_{BST}$ ).

**ABSOLUTE MAXIMUM RATINGS** <sup>(1)</sup>

$V_{IN}$ .....	-0.3V to +40V
$V_{SW}$ .....	-0.3V (-5V for <10ns) to $V_{IN\_MAX} + 0.3V$
$V_{BST}$ .....	$V_{SW\_MAX} + 6V$
All other pins .....	-0.3V to 6V
Continuous power dissipation ( $T_A = 25^\circ C$ ) <sup>(2)</sup> <sup>(5)</sup>	2.2W
Operating junction temperature ( $T_J$ ).....	150°C
Lead temperature .....	260°C
Storage temperature .....	-65°C to +150°C

**Recommended Operating Conditions** <sup>(3)</sup>

Supply voltage ( $V_{IN}$ ) .....	4.2V to 32V
Output voltage ( $V_{OUT}$ )..	0.6V to $V_{IN} \times D_{MAX}$ or 30V
Operating junction temp ( $T_J$ )....	-40°C to +125°C

**Thermal Resistance**

	$\theta_{JA}$	$\theta_{JB}$
TSOT23-6		
JEDEC <sup>(4)</sup> .....	97.3	25
EVL2462-J-00B <sup>(5)</sup> .....	57.3	
	$\theta_{JC\_TOP}$	$\theta_{JC\_BOT}$
JEDEC <sup>(4)</sup> .....	45.5	8.5
	$\psi_{JT}$	
JEDEC <sup>(4)</sup> .....	7.7	
EVL2462-J-00B <sup>(5)</sup> .....	12.6	

**Notes:**

- Exceeding these ratings may damage the device.
- The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_J$  (MAX), the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable continuous power dissipation at any ambient temperature is calculated by  $P_D$  (MAX) =  $(T_J$  (MAX) -  $T_A$ ) /  $\theta_{JA}$ . Exceeding the maximum allowable power dissipation can generate an excessive die temperature, which may cause the regulator to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- The device is not guaranteed to function outside of its operating conditions.
- The  $\theta_{JA}$  value is only valid for comparison with other packages and cannot be used for design purposes. This value is based on a JEDEC51-7 board. They do not represent the performance obtained in an actual application.
- Measured on a 2-layer, 2oz EVL2462-J-00B (5.1cmx5.1cm). The junction-to-top characterization parameter,  $\psi_{JT}$ , estimates the junction temperature in the real system based on the following equation:  $T_J = \psi_{JT} \times P_{LOSS} + T_{CASE\_TOP}$ , where  $P_{LOSS}$  is the entire loss of the IC in real application, and  $T_{CASE\_TOP}$  is the case top temperature.

## ELECTRICAL CHARACTERISTICS

$V_{IN} = 24V$ ,  $V_{EN} = 2V$ ,  $T_J = -40^{\circ}C$  to  $+125^{\circ}C$  <sup>(6)</sup>, typical values are at  $T_J = 25^{\circ}C$ , unless otherwise noted.

Parameter	Symbol	Conditions	Min	Typ	Max	Units
<b>Input Power Supply</b>						
Input voltage range	$V_{IN}$		4.2		32	V
$V_{IN}$ under-voltage lockout (UVLO) rising threshold	$V_{IN\_UVLO}$		3.55	3.85	4.15	V
$V_{IN}$ UVLO threshold hysteresis	$V_{IN\_UVLO\_HYS}$			360		mV
<b>Supply Current</b>						
Quiescent supply current	$I_Q$	$V_{FB} = 0.65V$ , no switching		55	100	$\mu A$
Shutdown supply current	$I_{SD}$	$V_{EN} = 0V$			3	$\mu A$
<b>MOSFET</b>						
High-side MOSFET (HS-FET) on resistance	$R_{DS(ON)\_HS}$	$V_{BST} - V_{SW} = 5V$		160		m $\Omega$
Low-side MOSFET (LS-FET) on resistance	$R_{DS(ON)\_LS}$			80		m $\Omega$
Switch leakage current	$I_{SW\_LKG}$				1	$\mu A$
<b>Current Limit and Zero-Current Detection (ZCD)</b>						
High-side (HS) switching peak current limit	$I_{LIMIT\_HS}$	Duty cycle = 42%	2.1	2.8	3.6	A
Low-side (LS) switching valley-current limit	$I_{LIMIT\_LS}$		1.85	2.4	2.95	A
Short hiccup duty cycle <sup>(7)</sup>	$D_{HICCUP}$			11.5		%
ZCD current	$I_{ZCD}$	$V_{OUT} = 5V$ , $L = 15\mu H$		50		mA
<b>Reference and Soft Start (SS)</b>						
Feedback (FB) voltage	$V_{FB}$	$T_J = 25^{\circ}C$	596	600	604	mV
		$T_J = -40^{\circ}C$ to $+125^{\circ}C$	594	600	606	mV
FB current	$I_{FB}$	$V_{FB} = 0.65V$	-50	0	+50	nA
Internal SS time	$t_{SS}$	$V_{OUT} = 0\%$ to $100\%$		2.5		ms
<b>Switching Frequency and Minimum On/Off Timer</b>						
Switching frequency	$f_{SW}$		600	800	950	kHz
Minimum on time <sup>(7)</sup>	$t_{ON\_MIN}$			110		ns
Minimum off time <sup>(7)</sup>	$t_{OFF\_MIN}$			200		ns
<b>Enable (EN) and Under-Voltage Lockout (UVLO)</b>						
EN rising threshold	$V_{EN\_RISING}$		1.14	1.22	1.3	V
EN hysteresis	$V_{EN\_HYS}$			220		mV
EN pull-down resistor	$R_{EN\_PD}$			1		M $\Omega$
<b>Protection</b>						
Output under-voltage protection (UVP) threshold	$V_{UVP}$	Hiccup entry	35	40	45	% of $V_{REF}$

**ELECTRICAL CHARACTERISTICS (continued)**

$V_{IN} = 24V$ ,  $V_{EN} = 2V$ ,  $T_J = -40^{\circ}C$  to  $+125^{\circ}C$  <sup>(6)</sup>, typical values are at  $T_J = 25^{\circ}C$ , unless otherwise noted.

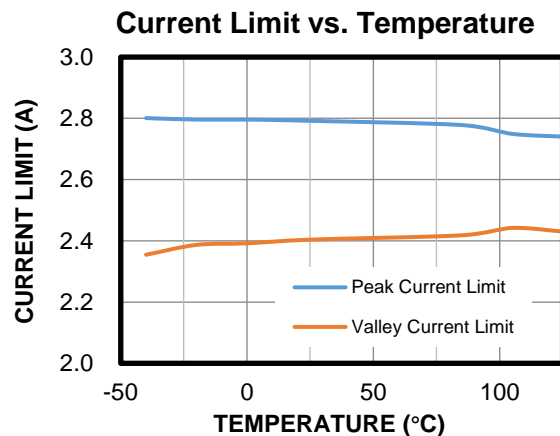
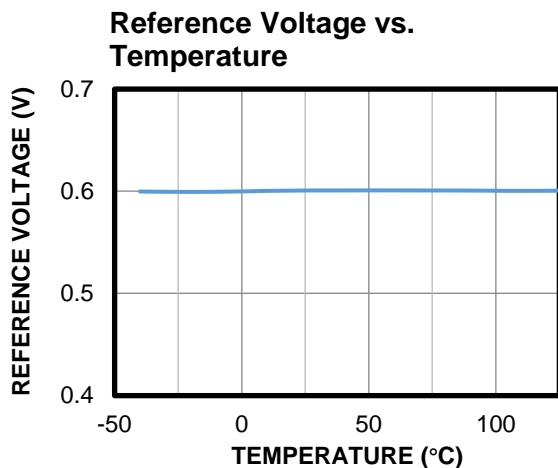
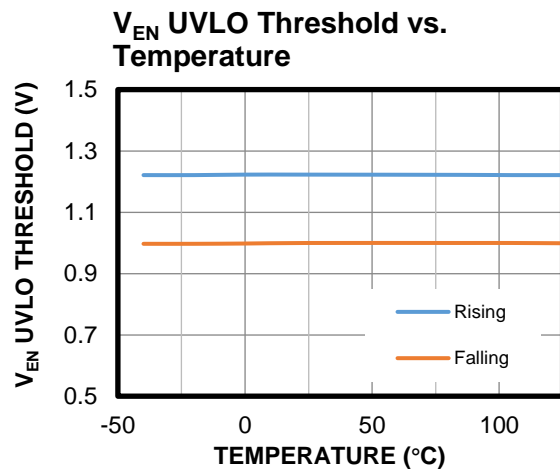
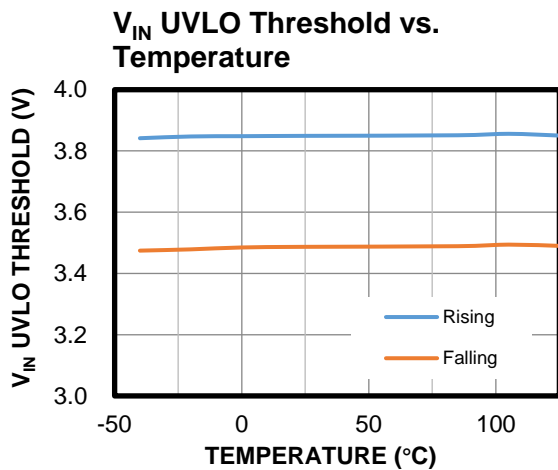
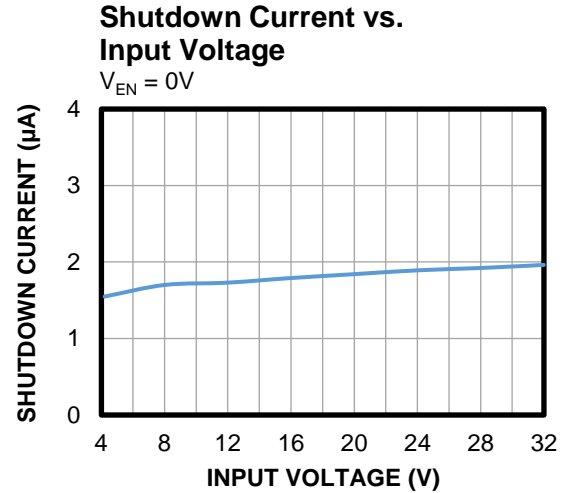
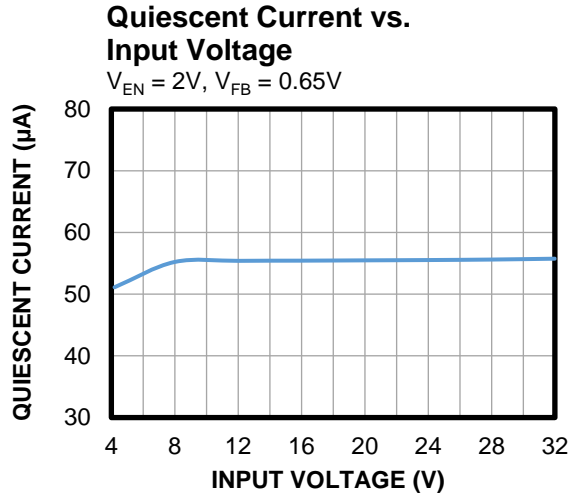
Parameter	Symbol	Conditions	Min	Typ	Max	Units
Output over-voltage protection (OVP) rising threshold	$V_{OVP\_R}$		110	115	120	% of $V_{REF}$
Output OVP threshold hysteresis	$V_{OVP\_HYS}$			10		% of $V_{REF}$
Output over-voltage (OV) delay	$t_{OVP\_DELAY}$			2		$\mu s$
Discharge resistor	$R_{DSC}$	OVP or shutdown through EN discharges on SW		150		$\Omega$
Thermal shutdown <sup>(7)</sup>	$T_{SD}$			150		$^{\circ}C$
Thermal hysteresis <sup>(7)</sup>	$T_{SD\_HYS}$			20		$^{\circ}C$

**Notes:**

- 6) Not tested in production and derived by the over-temperature correlation.  
 7) Not tested in production and derived by sample characterization.

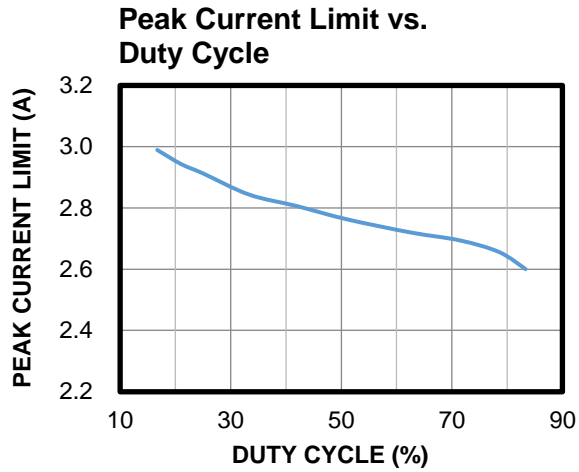
## TYPICAL CHARACTERISTICS

$V_{IN} = 24V$ ,  $T_A = 25^\circ C$ , unless otherwise noted.



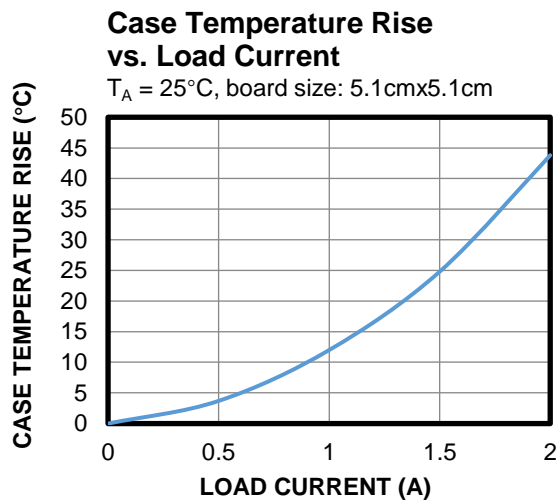
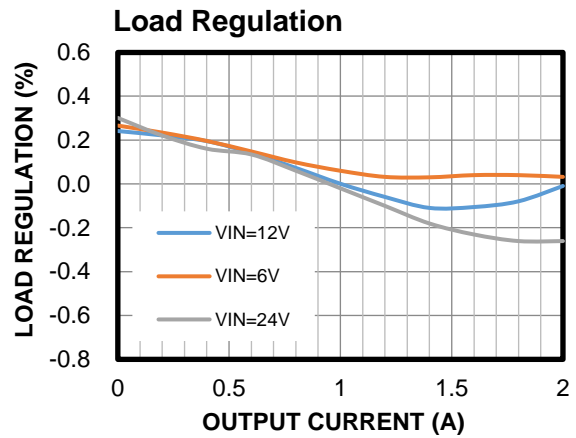
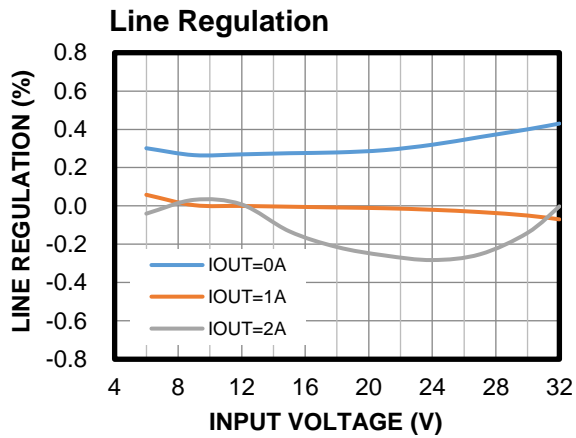
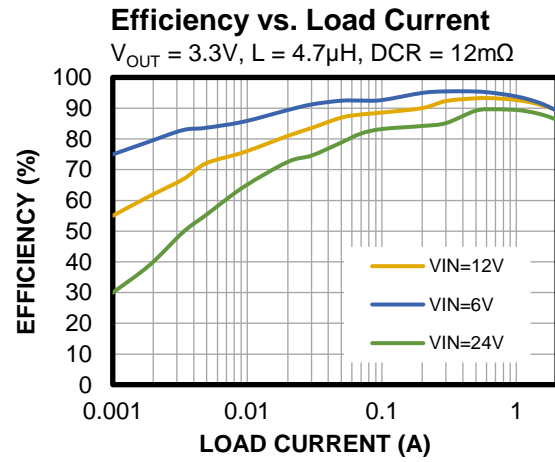
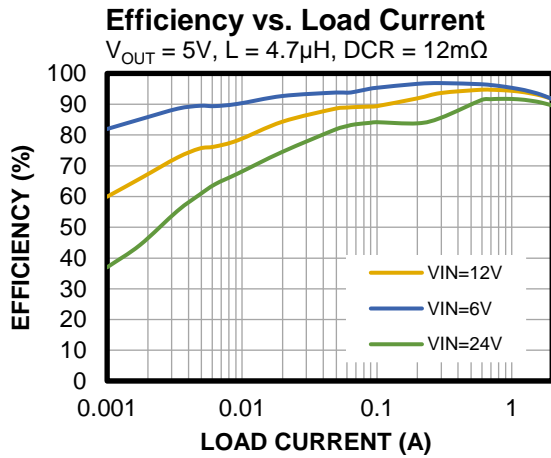
**TYPICAL CHARACTERISTICS (continued)**

$V_{IN} = 24V$ ,  $T_A = 25^\circ C$ , unless otherwise noted.



## TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $L = 4.7\mu H$ ,  $f_{SW} = 800kHz$ ,  $T_A = 25^\circ C$ , unless otherwise noted.

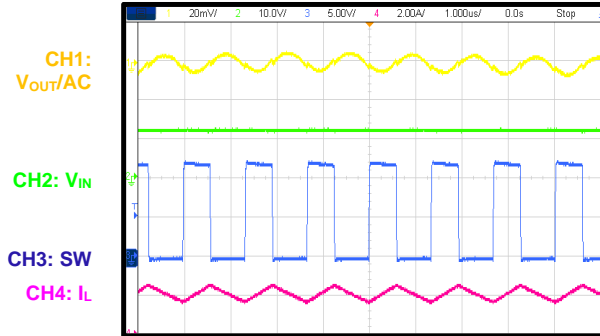


**TYPICAL PERFORMANCE CHARACTERISTICS (continued)**

$V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $L = 4.7\mu H$ ,  $f_{SW} = 800kHz$ ,  $T_A = 25^\circ C$ , unless otherwise noted.

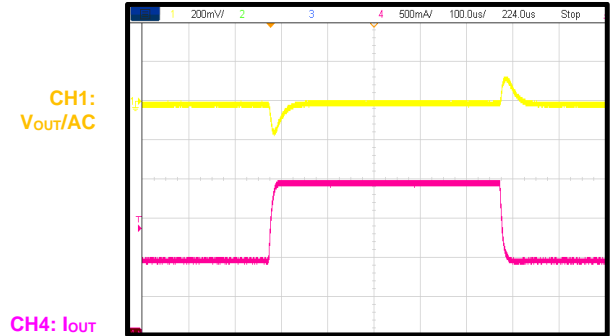
**Output Ripple**

$I_{OUT} = 2A$



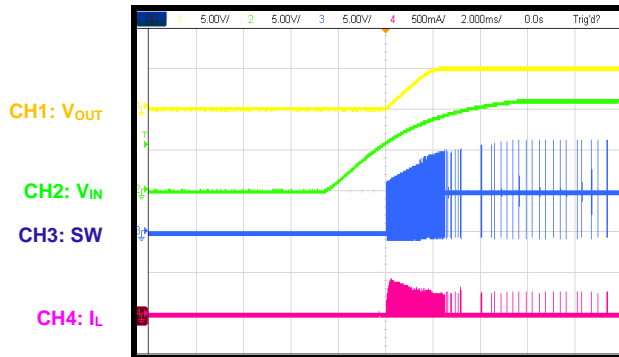
**Load Transient Response**

$I_{OUT} = 1A$  to  $2A$ , slew rate =  $2.5A/\mu s$  with e-load



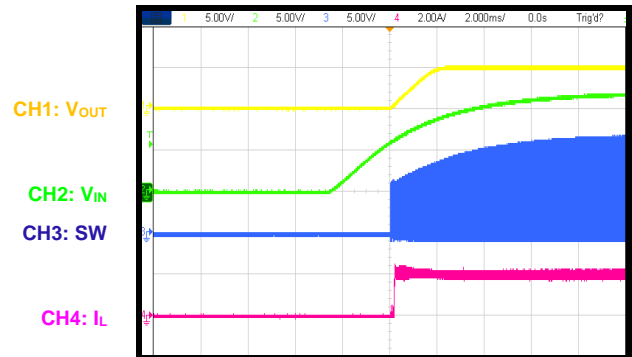
**Start-Up through VIN**

$I_{OUT} = 0A$



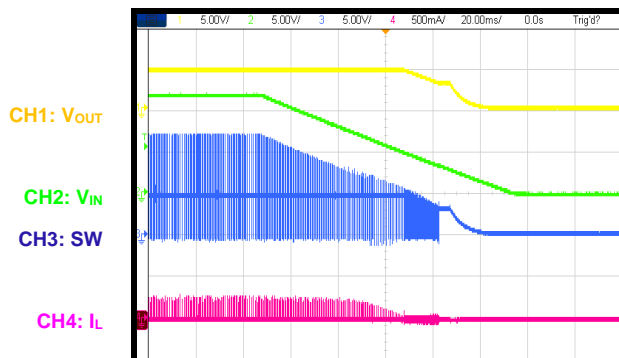
**Start-Up through VIN**

$I_{OUT} = 2A$



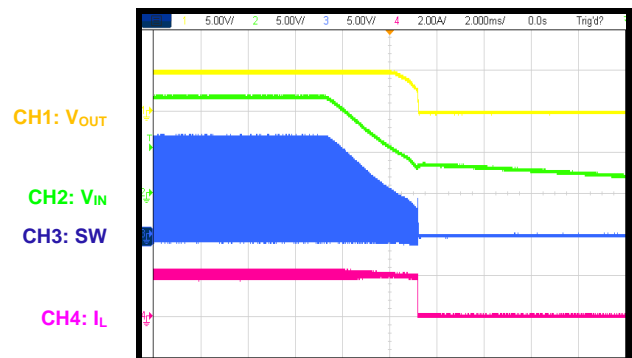
**Shutdown through VIN**

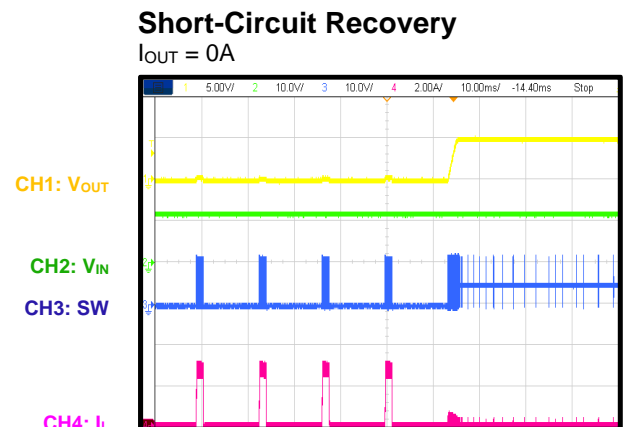
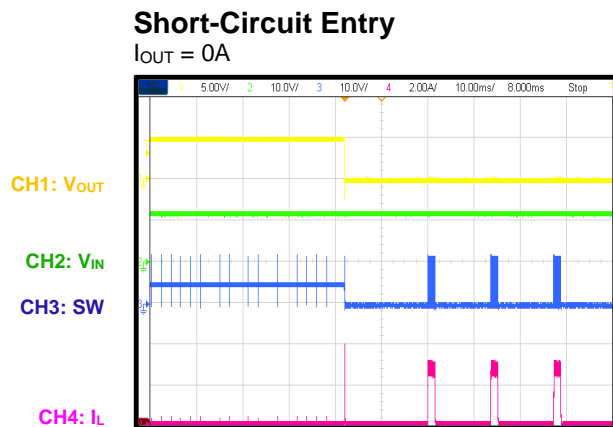
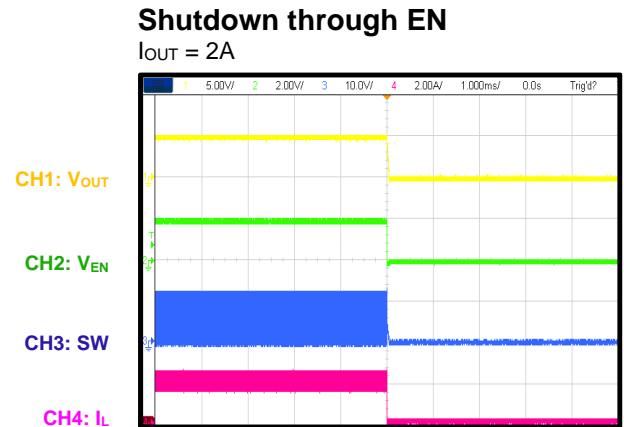
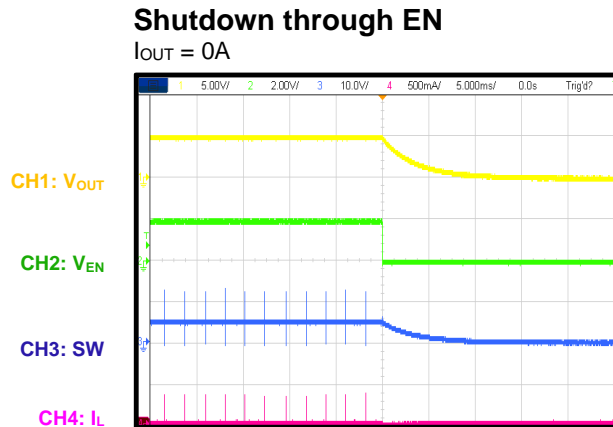
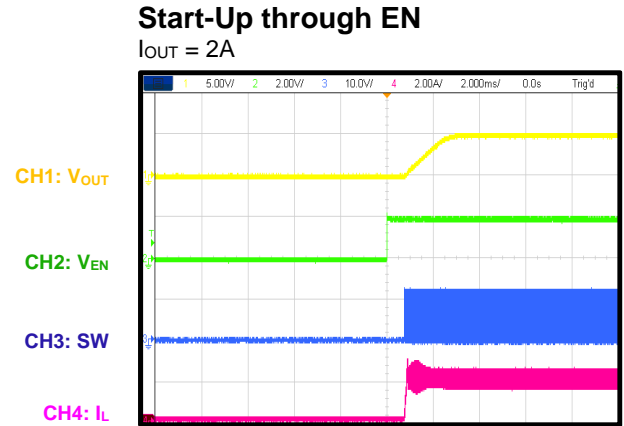
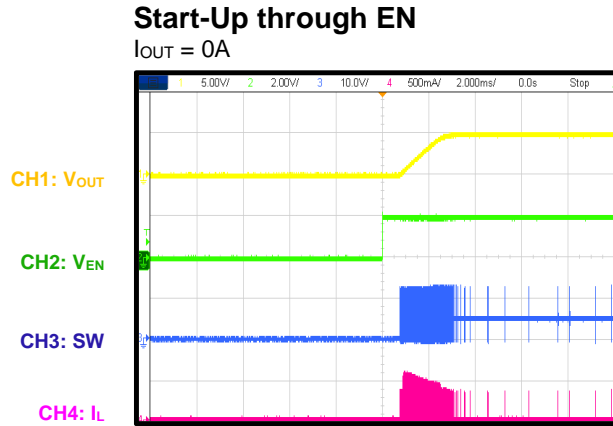
$I_{OUT} = 0A$



**Shutdown through VIN**

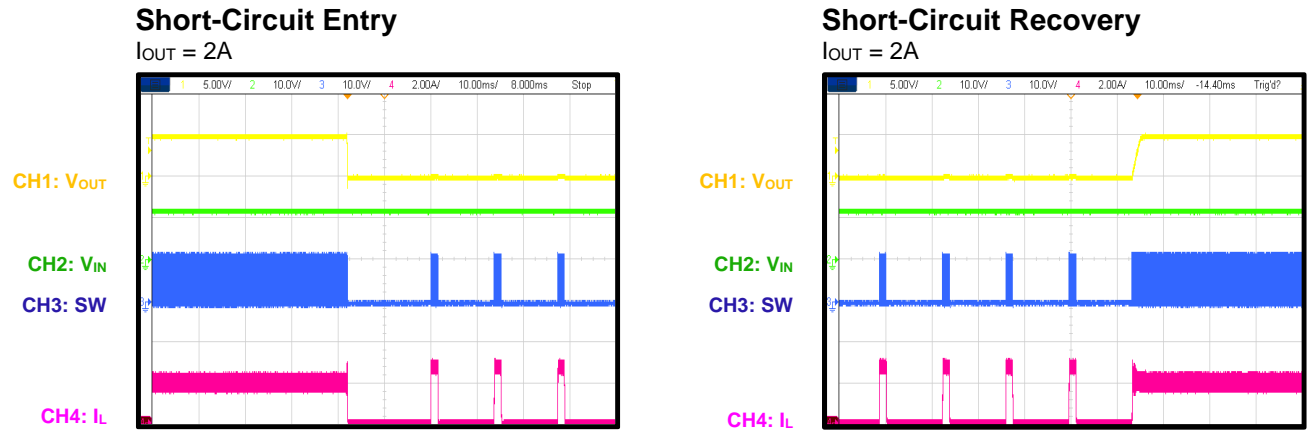
$I_{OUT} = 2A$



**TYPICAL PERFORMANCE CHARACTERISTICS (continued)**
 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $L = 4.7\mu H$ ,  $f_{SW} = 800kHz$ ,  $T_A = 25^\circ C$ , unless otherwise noted.


## TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

$V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $L = 4.7\mu H$ ,  $f_{SW} = 800kHz$ ,  $T_A = 25^\circ C$ , unless otherwise noted.



### FUNCTIONAL BLOCK DIAGRAM

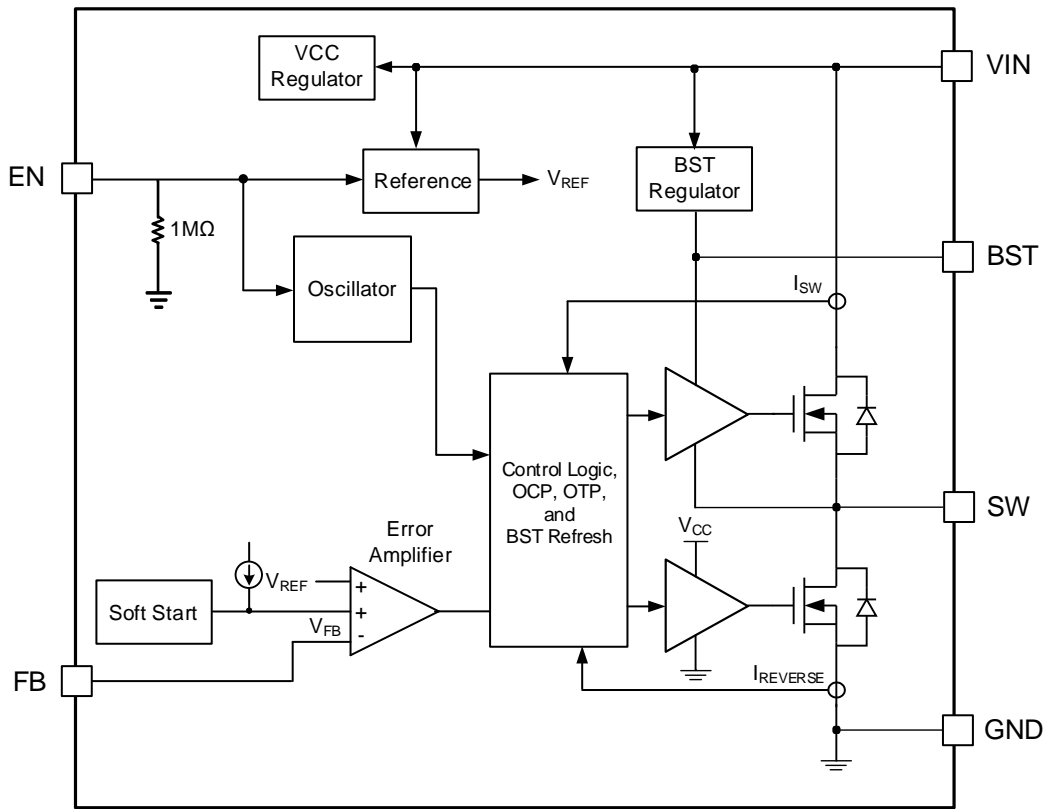


Figure 1: Functional Block Diagram

## OPERATION

The MP2462 is a synchronous, step-down switching regulator with integrated, internal high-side and low-side power MOSFETs (HS-FETs and LS-FETs, respectively). It provides 2A of highly efficient output current ( $I_{OUT}$ ) with current mode control. Its very low operational quiescent current ( $I_Q$ ) makes the device well-suited for battery-powered applications.

### Pulse-Width Modulation (PWM) Control

At moderate to high output currents, the MP2462 operates in a fixed-frequency, peak current control mode to regulate the output voltage ( $V_{OUT}$ ). A pulse-width modulation (PWM) cycle is initiated by the internal clock. At the clock's rising edge, the HS-FET turns on until its current reaches the value set by the COMP voltage ( $V_{COMP}$ ). When the HS-FET is off, the LS-FET turns on until the next cycle begins.

If the current in the HS-FET does not reach the current set via  $V_{COMP}$  within one PWM period, then the HS-FET remains on.

### Advanced Asynchronous Modulation (AAM) Mode

The MP2462 employs advanced asynchronous modulation (AAM) mode to optimize efficiency during light-load or no-load conditions.

The device first enters asynchronous operation while the inductor current ( $I_L$ ) approaches 0A at light loads. If the load further decreases or there is no load, then  $V_{COMP}$  drops below the AAM mode voltage ( $V_{AAM}$ ), and the MP2462 enters AAM mode or sleep mode, which consumes very low  $I_Q$  and improves light-load efficiency.

In AAM mode, the internal clock is reset whenever  $V_{COMP}$  exceeds  $V_{AAM}$ , and the crossover time is taken as the benchmark for the next clock. If the load increases, and the  $V_{COMP}$  DC value exceeds  $V_{AAM}$ , then the device enters discontinuous conduction mode (DCM) or continuous conduction mode (CCM), which have a constant switching frequency ( $f_{SW}$ ).

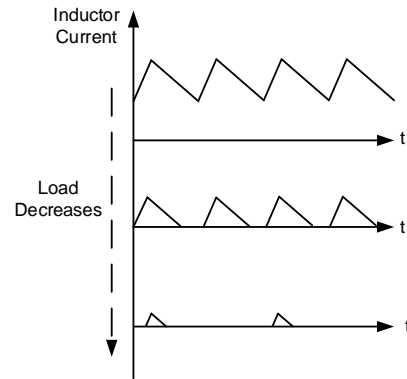


Figure 2: AAM Mode and PWM Mode

### Error Amplifier (EA)

The error amplifier (EA) is comprised of an internal operation amplifier (op amp) with an RC feedback network connected between its output node (internal COMP node) and its negative input node (FB). If the FB voltage ( $V_{FB}$ ) drops below the internal reference voltage ( $V_{REF}$ ), then the op amp pulls the COMP output high, generating a higher switch peak current output and delivering more energy to the output. Conversely, if  $V_{FB}$  rises, then the switch peak current output drops.

### Bootstrap (BST) Charging

The bootstrap (BST) capacitor ( $C_{BST}$ ) is charged and regulated to about 5V via the dedicated internal BST regulator. When the HS-FET is on, the input voltage ( $V_{IN}$ ) is about equal to the SW pin voltage ( $V_{SW}$ ), meaning  $C_{BST}$  cannot be charged.

At higher duty cycle operation conditions, the time period available to BST charging is less. This means that  $C_{BST}$  may not be charged sufficiently. If the internal circuit does not have sufficient voltage or time to charge  $C_{BST}$ , then additional external circuitry can be used to ensure that the BST voltage ( $V_{BST}$ ) is within the normal operation region.

### Low-Dropout (LDO) Operation

To improve dropout, the MP2462 is designed to extend the on time ( $t_{ON}$ ) when the minimum off time ( $t_{OFF\_MIN}$ ) is reached. When the HS-FET on time is extended, the frequency drops. The MP2462 can support a maximum 98% duty cycle with a 100kHz minimum frequency.

### Enable (EN) Control

EN is a digital control pin that turns the regulator on and off. Pull EN high to turn on the regulator; pull the pin low to turn the regulator off. An internal 1M $\Omega$  resistor between EN and GND allows EN to be floated, which shuts down the chip. The MP2462 provides an accurate EN threshold, meaning a resistor divider between VIN and GND can configure VIN, at which the MP2462 is enabled. This is highly recommended for applications where there is no dedicated EN logic signal.

The pull-up resistor ( $R_{UP}$ ) and pull-down resistor ( $R_{DOWN}$ ) should be selected to ensure that the EN pin voltage ( $V_{EN}$ ) does not exceed 5.5V if  $V_{IN}$  reaches its maximum.

EN can also be connected to VIN directly via  $R_{UP}$ . To avoid excess sink current on the EN pin,  $R_{UP}$  is typically between 1M $\Omega$  and 2M $\Omega$ . A typical  $R_{UP}$  is 1M $\Omega$ .

If EN is connected directly to a voltage source without any  $R_{UP}$  requirements, then the voltage source amplitude must be limited to  $\leq 5.5V$ .

To avoid noise on EN, place a 0.1 $\mu F$  ceramic capacitor as close to the EN and GND pins as possible.

### Under-Voltage Lockout (UVLO)

Under-voltage lockout (UVLO) protects the chip from operating at an insufficient supply voltage. The VIN UVLO rising threshold is about 3.85V, while the VIN UVLO falling threshold is about 3.49V.

### Internal Soft Start (SS)

Soft start (SS) prevents the output voltage ( $V_{OUT}$ ) from overshooting during start-up. When the chip starts up, the internal circuit generates a soft-start voltage ( $V_{SS}$ ) that ramps up from 0V to 1V during the SS time ( $t_{SS}$ ). If  $V_{SS}$  is below  $V_{REF}$ , then  $V_{SS}$  overrides  $V_{REF}$ , meaning the EA uses  $V_{SS}$  as the reference; if  $V_{SS}$  exceeds  $V_{REF}$ , then the EA continues using  $V_{REF}$  as its reference.  $t_{SS}$  is internally set to 2.5ms.

### Pre-Biased Start-Up

The MP2462 is designed for monotonic start-up into pre-biased loads. If the output is pre-biased to a certain voltage during start-up, then  $V_{BST}$  is refreshed and charged. The voltage on the soft-start capacitor ( $C_{SS}$ ) is charged as well. If  $V_{BST}$

exceeds its rising threshold, and the internal  $V_{SS}$  exceeds the sensed  $V_{OUT}$  at FB, then the device enters normal operation.

### Thermal Shutdown

Thermal shutdown is implemented to prevent the chip from running away thermally. If the silicon die temperature exceeds its upper threshold, then the power MOSFETs shut down. If the temperature is below its lower threshold, then thermal shutdown is removed, and the chip is enabled again.

### Output Discharge

The MP2462 discharges the output when the controller is turned off by the protection functions, including over-voltage protection (OVP) and shutdown through EN. The discharge resistor on the output is typically 150 $\Omega$ .

### Current Comparator and Current Limit

The power MOSFET current is sensed accurately via a current-sense MOSFET. The current is fed to the high-speed current comparator for current-mode control purposes. The current comparator uses this sensed current as one of its inputs. When the HS-FET turns on, the comparator is first blanked until the end of the turn-on transition to avoid noise. Then the comparator compares the power switch current with  $V_{COMP}$ . If the sensed current exceeds  $V_{COMP}$ , then the comparator outputs low to turn off the HS-FET.

The internal power MOSFET's maximum current is limited cycle-by-cycle internally.

### Hiccup Protection

If the output is shorted to ground, causing  $V_{OUT}$  to drop below 40% of its nominal output, then the IC shuts down momentarily and begins discharging  $C_{SS}$ . The IC restarts with a full soft start once  $C_{SS}$  is fully discharged. This hiccup process is repeated until the fault is removed.

### Start-Up and Shutdown

If both  $V_{IN}$  and  $V_{EN}$  exceed their respective thresholds, then the chip starts up. The reference block starts first, generating stable reference voltages and currents, then the internal regulator is enabled. The regulator provides a stable supply for the remaining circuitries.

While the internal supply rail starts up, an internal timer holds the power MOSFET off to blank the start-up glitches. When the SS block is enabled, it first holds the SS output low to ensure that the remaining circuitries are ready, then slowly ramps up.

Three events can shut down the chip:  $V_{EN}$  going low,  $V_{IN}$  going low, and thermal shutdown.

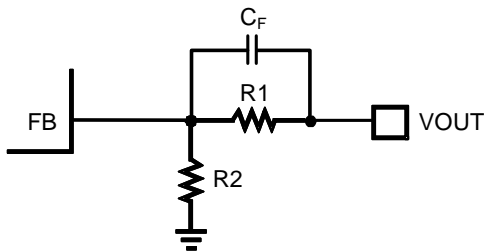
## APPLICATION INFORMATION

### Setting the Output

The external resistor divider sets the output voltage ( $V_{OUT}$ ). First, select a value for  $R_2$ , where  $R_2$  should be chosen reasonably. A small  $R_2$  results in considerable quiescent current ( $I_Q$ ) loss, while a too-large  $R_2$  makes the FB noise sensitive. Typically, set the current through  $R_2$  between  $5\mu A$  and  $100\mu A$  to achieve a good balance between system stability and no-load loss. Then  $R_1$  can be calculated with Equation (1):

$$R_1 = \frac{V_{OUT} - V_{REF}}{V_{REF}} \times R_2 \quad (1)$$

The feedback network is highly recommended (see Figure 3).



**Figure 3: Feedback Network**

Table 1 shows the recommended feedback network parameters for common output voltages. The minimum on time ( $t_{MIN\_ON}$ ) must not be triggered in application; otherwise, this leads to instability since frequency foldback only works during the start-up period.

**Table 1: Recommended Parameters for Common Output Voltages <sup>(8)</sup>**

$V_{OUT}$ (V)	$R_1$ (k $\Omega$ )	$R_2$ (k $\Omega$ )	$C_F$ (pF)	$L$ ( $\mu$ H)
5	150	20.5	8.2	4.7
3.3	150	33.2	8.2	4.7

**Note:**

8) Based on  $V_{IN} = 12V$ , a different  $V_{IN}$ , output inductance, and output capacitance may affect the selection of  $R_1$ ,  $R_2$ , and  $C_F$ . For additional component parameters, see the Typical Application Circuits section on page 19.

### Selecting the Inductor

**Optimized Performance with  
MPS Inductor MPL-AL6060 Series**

For most applications, use an inductor with a DC current rating at least 25% higher than the maximum load current ( $I_{LOAD\_MAX}$ ). For the

highest efficiency, use an inductor with a DC resistance less than  $15m\Omega$ .

For most designs, the inductance ( $L$ ) can be calculated with Equation (2):

$$L = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} \times \Delta I_L \times f_{SW}} \quad (2)$$

Where  $\Delta I_L$  is the inductor ripple current.

Choose the inductor ripple current at about 30% to 60% of  $I_{LOAD\_MAX}$ . The maximum inductor peak current ( $I_{L\_MAX}$ ) can be calculated with Equation (3):

$$I_{L\_MAX} = I_{LOAD} + \frac{\Delta I_L}{2} \quad (3)$$

MPS inductors are optimized and tested for use with our complete line of integrated circuits.

Table 2 shows the recommended power inductors, where the part number can be selected based on the design requirements.

**Table 2: Power Inductor Selection**

Part Number	Inductance	Manufacturer
MPL-AL6060-4R7	4.7 $\mu$ H	MPS

For more information, visit the Inductors pages on the MPS website.

### Selecting the Input Capacitor

The step-down converter has a discontinuous input current ( $I_{IN}$ ) and requires a capacitor to supply AC current while maintaining the DC input voltage. For optimal performance, use low-ESR capacitors. Ceramic capacitors with X5R or X7R dielectrics are recommended because of their low ESR and small temperature coefficients. For most applications, use two  $10\mu F$  capacitors.

Since the input capacitor ( $C_1$ , also called  $C_{IN}$ ) absorbs the input switching current, it requires an adequate ripple current rating. The RMS current in  $C_{IN}$  ( $I_{C1}$ ) can be estimated with Equation (4):

$$I_{C1} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)} \quad (4)$$

The worst-case condition occurs at  $V_{IN} = 2 \times V_{OUT}$ , which can be calculated with Equation (5):

$$I_{C1} = \frac{I_{LOAD}}{2} \quad (5)$$

For simplification, choose C1 with an RMS current rating that is greater than half of  $I_{LOAD\_MAX}$ .

C1 can be electrolytic, tantalum, or ceramic. When using electrolytic or tantalum capacitors, a small, high-quality ceramic capacitor (e.g. 0.1µF) should be placed as close to the IC as possible. When using ceramic capacitors, ensure that they have enough capacitance to provide a sufficient charge to prevent excessive voltage ripple at the input.

The input voltage ripple ( $\Delta V_{IN}$ ) caused by the capacitance can be estimated with Equation (6):

$$\Delta V_{IN} = \frac{I_{LOAD}}{f_{SW} \times C1} \times \frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \quad (6)$$

### Selecting the Output Capacitor

The output capacitor (C2, also called  $C_{OUT}$ ) maintains the DC output voltage. Use ceramic, tantalum, or low-ESR electrolytic capacitors. For the best results, use low-ESR capacitors to maintain a low output voltage ripple. The output voltage ripple ( $\Delta V_{OUT}$ ) can be estimated with Equation (7):

$$\Delta V_{OUT} = \frac{V_{OUT}}{f_{SW} \times L} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \times \left(R_{ESR} + \frac{1}{8 \times f_{SW} \times C2}\right) \quad (7)$$

Where  $R_{ESR}$  is the C2 equivalent series resistance (ESR).

For ceramic capacitors, the capacitance dominates the impedance at the switching frequency ( $f_{SW}$ ), and the capacitance causes the majority of  $\Delta V_{OUT}$ . For simplification,  $\Delta V_{OUT}$  can be estimated with Equation (8):

$$\Delta V_{OUT} = \frac{V_{OUT}}{8 \times f_{SW}^2 \times L \times C2} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \quad (8)$$

For tantalum or electrolytic capacitors, the ESR dominates the impedance at  $f_{SW}$ . For simplification,  $\Delta V_{OUT}$  can be estimated with Equation (9):

$$\Delta V_{OUT} = \frac{V_{OUT}}{f_{SW} \times L} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \times R_{ESR} \quad (9)$$

The C2 characteristics affect the stability of the regulation system. The MP2462 can be optimized for a wide range of capacitances and ESR values.

### Design Example

Table 3 shows a design example where ceramic capacitors are applied.

**Table 3: Design Example**

$V_{IN}$	$V_{OUT}$	$I_{OUT}$
12V	5V	2A

Figure 5 and Figure 6 on page 19 show the detailed application schematics. See the Typical Characteristics section on page 6 for the typical performance and waveforms. For more device applications, refer to the EVL2462-J-00B datasheet.

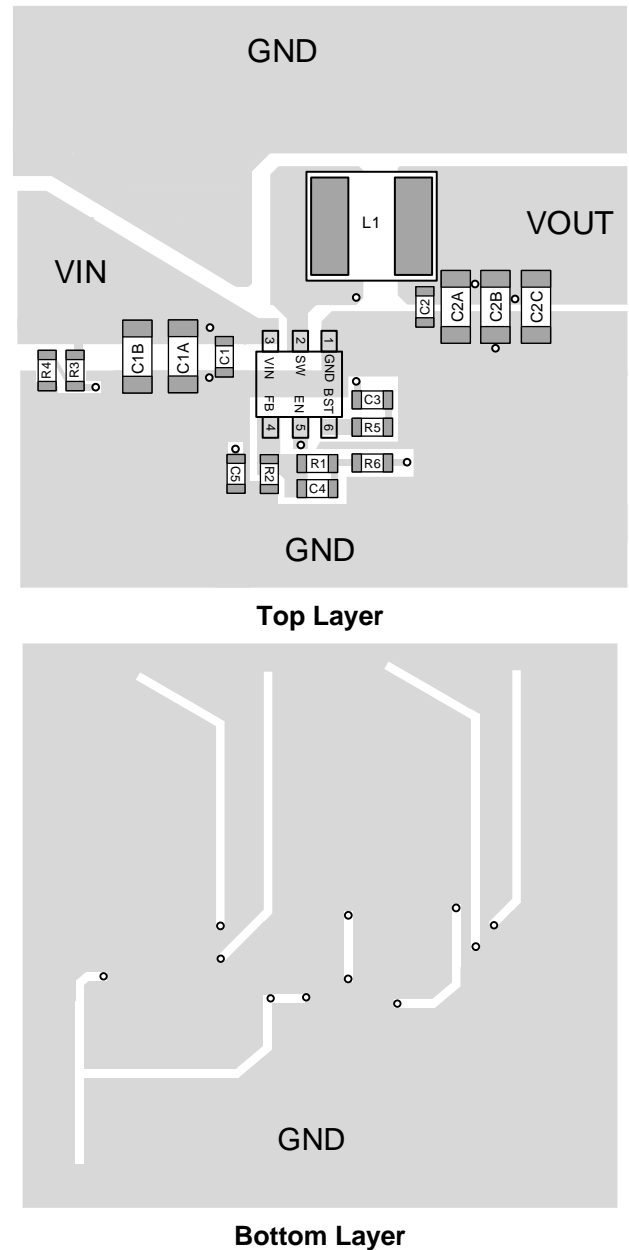
**PCB Layout Guidelines <sup>(9)</sup>**

Proper layout, especially of the switching power supplies, is critical for stable operation. Poor layout design can result in poor line or load regulation and stability issues. For the best results, refer to Figure 4 and follow the guidelines below:

1. Keep the connection between the input ground and GND as short and wide as possible.
2. Keep the connection between C1 and VIN as short and wide as possible.
3. Ensure all feedback connections are short and direct.
4. Place the feedback resistors and compensation components as close to the chip as possible.
5. Route SW away from sensitive analog areas such as FB.
6. Place the BST capacitor ( $C_{BST}$ ) as close to the BST and SW pins as possible.

**Note:**

- 9) The recommended layout is based on the Typical Application Circuits section on page 19.


**Figure 4: Recommended PCB Layout**

TYPICAL APPLICATION CIRCUITS

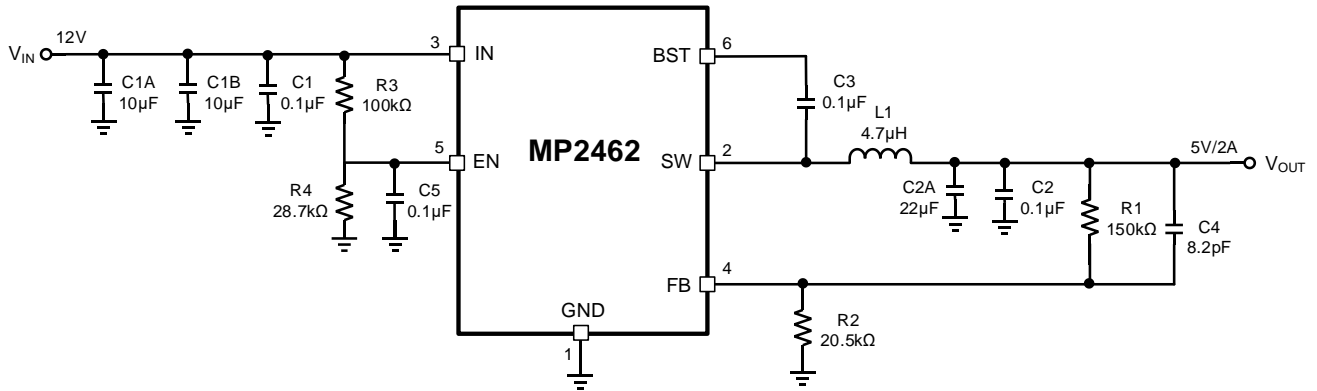


Figure 5: Typical Application Circuit (5V Output)

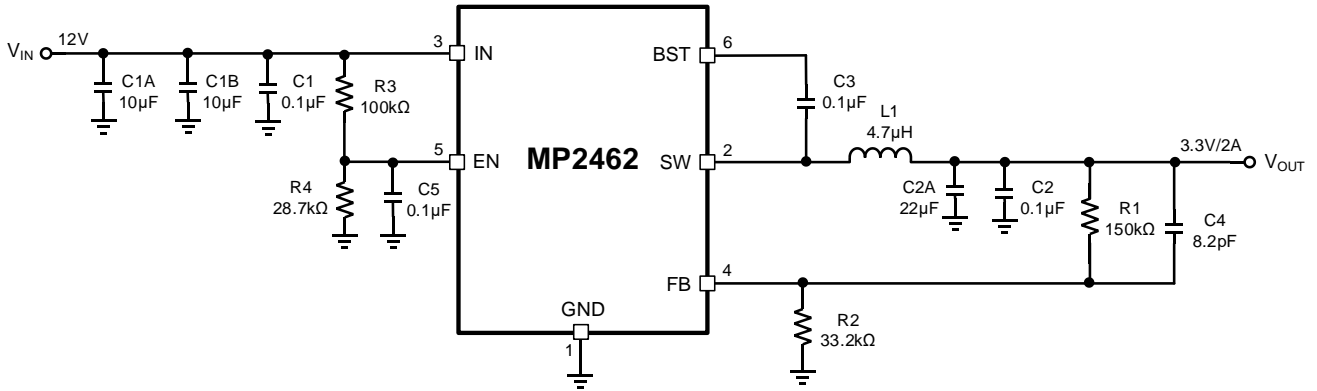
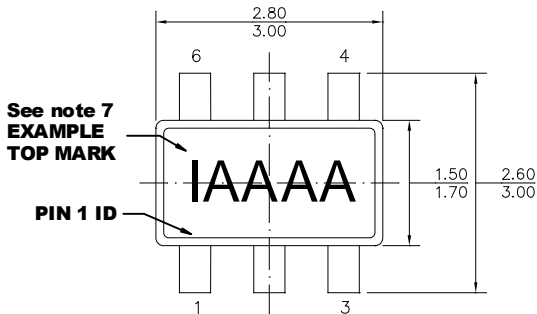


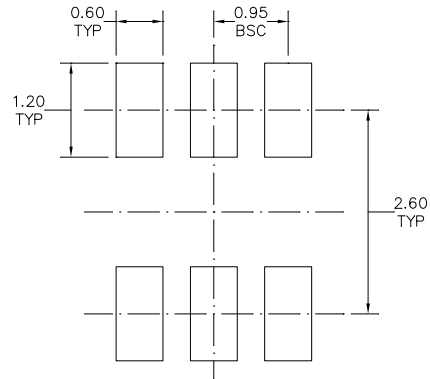
Figure 6: Typical Application Circuit (3.3V Output)

PACKAGE INFORMATION

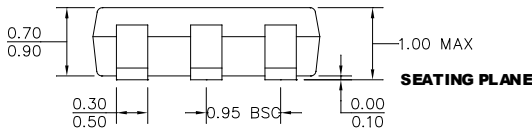
TSOT23-6



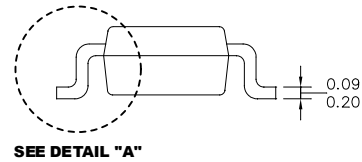
**TOP VIEW**



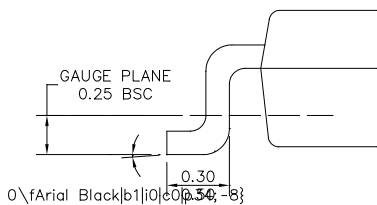
**RECOMMENDED LAND PATTERN**



**FRONT VIEW**



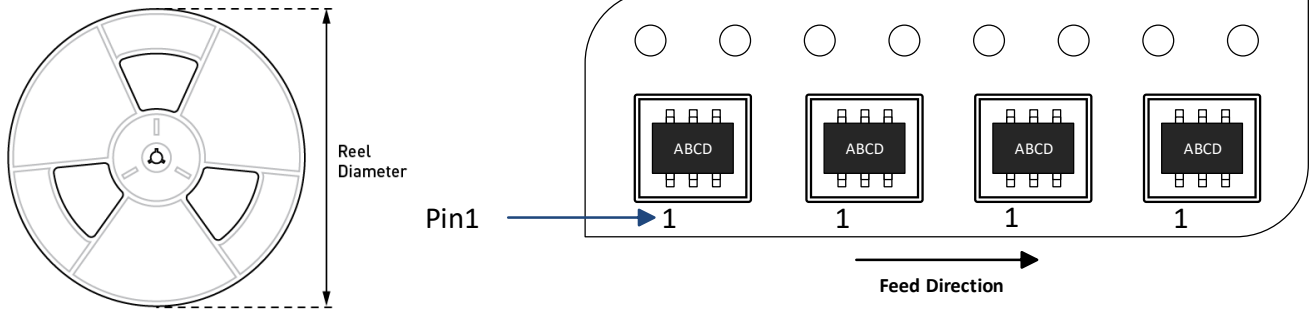
**SIDE VIEW**



**DETAIL "A"**

**NOTE:**

- 1) ALL DIMENSIONS ARE IN MILLIMETERS.
- 2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH, PROTRUSION OR GATE BURR.
- 3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION.
- 4) LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.10 MILLIMETERS MAX.
- 5) DRAWING CONFORMS TO JEDEC MO-193, VARIATION AB.
- 6) DRAWING IS NOT TO SCALE.
- 7) PIN 1 IS LOWER LEFT PIN WHEN READING TOP MARK FROM LEFT TO RIGHT, (SEE EXAMPLE TOP MARK)

**CARRIER INFORMATION**


Part Number	Package Description	Quantity/ Reel	Quantity/ Tube	Quantity/ Tray	Reel Diameter	Carrier Tape Width	Carrier Tape Pitch
MP2462GJ-Z	TSOT23-6	3000	N/A	N/A	7in	8mm	4mm

## REVISION HISTORY

Revision #	Revision Date	Description	Pages Updated
1.0	9/24/2025	Initial Release	-

**Notice:** The information in this document is subject to change without notice. Please contact MPS for current specifications. Users should warrant and guarantee that third-party Intellectual Property rights are not infringed upon when integrating MPS products into any application. MPS will not assume any legal responsibility for any said applications.