

### DESCRIPTION

The MP3414A is a high-efficiency, synchronous current mode, step-up converter with output disconnect.

The MP3414A can start up from an input voltage as low as 1.8V while providing inrush current limiting and output short-circuit protection (SCP). The integrated P-channel synchronous rectifier improves efficiency and eliminates the need for an external Schottky diode. The PMOS disconnects the output from the input when the MP3414A shuts down. The output disconnect feature allows the output to be discharged completely, allowing the MP3414A to draw a supply current of under 1 $\mu$ A in shutdown mode.

The 1MHz switching frequency allows small external components while the internal compensation and soft start minimize the external component count. These features produce a compact solution for a wide current load range.

The MP3414A features an integrated power MOSFET that supports an output of up to 5.5V and a peak switching current above 3A.

The MP3414A is available in a small 8-pin TSOT23 package.

### FEATURES

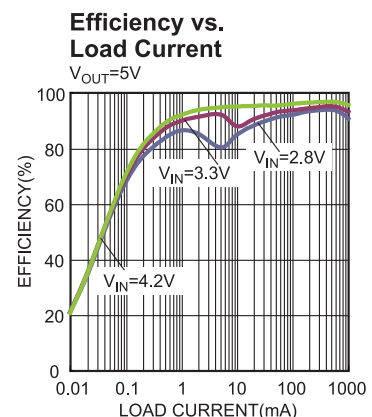
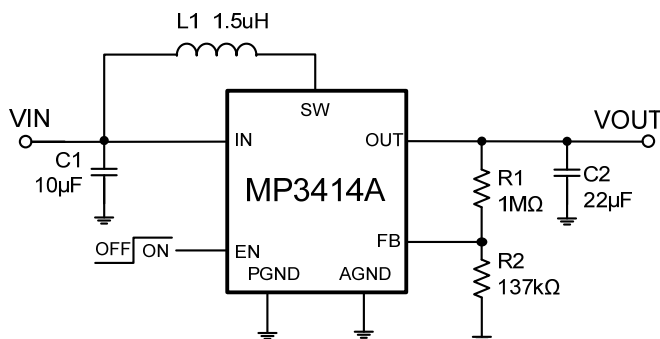
- Supports 5V/1A Output at 2.8V Input
- 1.8V to 5.5V Input Voltage Range
- Up to 5.5V Output Voltage
- Internal Synchronous Rectifier
- 1MHz Fixed Switching Frequency
- 22 $\mu$ A Quiescent Current
- <1 $\mu$ A Shutdown Current
- True Output Disconnect from Input
- Up to 97% Efficiency
- Internal Compensation, Inrush Current Limiting, and Internal Soft Start
- Tiny External Components
- OVP, SCP, and OTP
- TSOT23-8 Package

### APPLICATIONS

- Two-Cell and Three-Cell Alkaline, NiCd or NiMH, or Single-Cell Li Battery-Power Products
- Personal Medical Devices
- Portable Media Players
- Wireless Peripherals
- Gaming Accessories

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### TYPICAL APPLICATION



### ORDERING INFORMATION

Part Number*	Package	Top Marking
MP3414AGJ	TSOT23-8	See Below

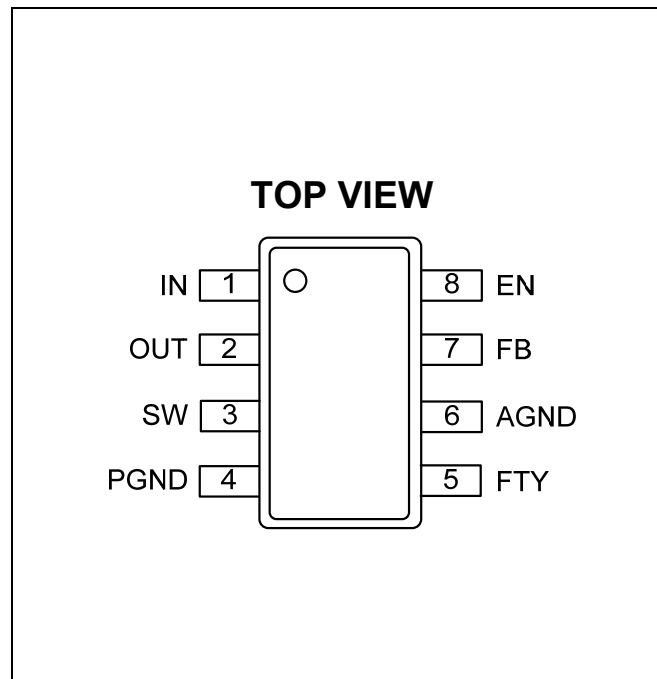
\* For Tape & Reel, add suffix -Z (e.g. MP3414AGJ-Z)

### TOP MARKING

**| AKTY**

AKT: Product code of MP3414AGJ  
Y: Year code

### PACKAGE REFERENCE



**ABSOLUTE MAXIMUM RATINGS** <sup>(1)</sup>

SW, OUT .....	-0.3V to +6.5V
SW (<5ns) .....	-1V to +9V
All other pins .....	-0.3V to +6.5V
Continuous power dissipation (T <sub>A</sub> = +25°C) <sup>(2)</sup>	1.25W
.....	1.25W
Junction temperature .....	150°C
Lead temperature .....	260°C
Storage temperature .....	-65°C to +150°C

**Recommended Operating Conditions** <sup>(3)</sup>

Supply voltage (V <sub>IN</sub> ) .....	1.8V to 5.5V
V <sub>OUT</sub> .....	V <sub>IN-MAX</sub> x 106% to 5.5V <sup>(4)</sup>
Operating junction temp. (T <sub>J</sub> )...	-40°C to +125°C

<b>Thermal Resistance</b> <sup>(5)</sup>	<b>θ<sub>JA</sub></b>	<b>θ<sub>JC</sub></b>	
TSOT23-8 .....	100	55	°C/W

**NOTES:**

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature T<sub>J</sub> (MAX), the junction-to-ambient thermal resistance θ<sub>JA</sub>, and the ambient temperature T<sub>A</sub>. The maximum allowable continuous power dissipation at any ambient temperature is calculated by P<sub>D</sub> (MAX) = (T<sub>J</sub> (MAX)-T<sub>A</sub>)/θ<sub>JA</sub>. Exceeding the maximum allowable power dissipation will produce an excessive die temperature, causing the regulator to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 3) The device is not guaranteed to function outside of its operating conditions.
- 4) If V<sub>IN</sub> is close to V<sub>OUT</sub>, the boost converter may trigger minimum on-time. When V<sub>IN</sub> is higher than V<sub>OUT</sub>, the boost converter will switch between boost mode and linear charge mode. Both conditions will result in a V<sub>OUT-RIPPLE</sub> that is too high. Therefore, this is not suggested.
- 5) Measured on JESD51-7, 4-layer PCB.

## ELECTRICAL CHARACTERISTICS

$V_{IN} = V_{EN} = 3.3V$ ,  $V_{OUT} = 5V$ ,  $T_J = -40^{\circ}C$  to  $125^{\circ}C$ , typical value is tested at  $T_J = 25^{\circ}C$ , unless otherwise noted.

Parameters	Symbol	Condition	Min	Typ	Max	Units
<b>Voltage Range</b>						
Quiescent current	$I_Q$	$V_{EN} = V_{IN} = 3.3V$ , $V_{OUT} = 5V$ , no load, $V_{FB} = 0.65V$ , measured on OUT, $T_J = 25^{\circ}C$		22	30	$\mu A$
		$V_{EN} = V_{IN} = 3.3V$ , $V_{OUT} = 5V$ , no load, $V_{FB} = 0.65V$ , measured on IN, $T_J = 25^{\circ}C$		8	12	$\mu A$
Shutdown current	$I_{SD}$	$V_{EN} = V_{OUT} = 0V$ , measured on IN $T_J = 25^{\circ}C$		0.1	1	$\mu A$
IN under-voltage lockout	$V_{IN\_UVLO}$	$V_{IN}$ rising, $T_J = 25^{\circ}C$ .		1.65	1.7	V
IN under-voltage lockout hysteresis				100		mV
<b>Step-Up Converter</b>						
Operation frequency	$F_{SW}$		0.8	1.0	1.2	MHz
Feedback voltage reference	$V_{FB}$	$T_J = 25^{\circ}C$	594	600	606	mV
		$T_J = -40^{\circ}C$ to $125^{\circ}C$	591	600	609	mV
Feedback input current	$I_{FB}$	$V_{FB} = 0.63V$		1	50	nA
NMOS on resistance	$R_{NDS\_ON}$			70		m $\Omega$
NMOS leakage current	$I_{N\_LK}$	$V_{SW} = 6.5V$ , $T_J = 25^{\circ}C$ .		0.1	1	$\mu A$
PMOS on resistance	$R_{PDS\_ON}$			80		m $\Omega$
PMOS leakage current	$I_{P\_LK}$	$V_{SW} = 6.5V$ , $V_{OUT} = 0V$ , $T_J = 25^{\circ}C$ .		0.1	1	$\mu A$
Maximum duty cycle	$D_{MAX}$		85	95		%
Start-up current limit	$I_{ST\_LIMIT}$	$V_{IN} = 4V$ , $V_o = 0V$		0.3		A
		$V_{IN} = 4V$ , $V_o$ setting = 3.6V, pull $V_o$ to 3.3V		0.8		A
NMOS current limit	$I_{SW\_LIMIT}$	Duty = 40%	3	3.6		A
<b>Logic Interface</b>						
EN input high-level voltage	$V_{EN\_H}$		1.2			V
EN input low-level voltage	$V_{EN\_L}$				0.4	V
EN input current	$I_{EN}$	Connect to $V_{IN}$		10		nA
<b>Protection</b>						
Thermal shutdown <sup>(6)</sup>				155		$^{\circ}C$
Over-temperature hysteresis <sup>(6)</sup>				25		$^{\circ}C$

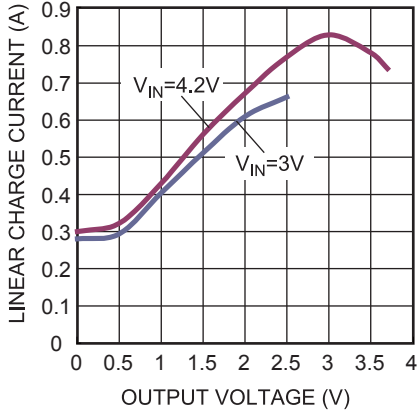
**NOTE:**

6) Guaranteed by characterization, not production tested.

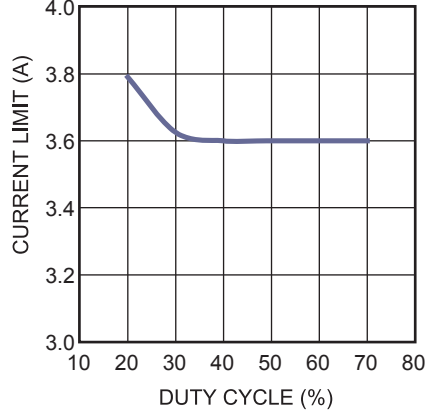
## TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 3.3V$ ,  $V_{OUT} = 5V$ ,  $L = 1.5\mu H$ ,  $T_A = 25^\circ C$ , unless otherwise noted.

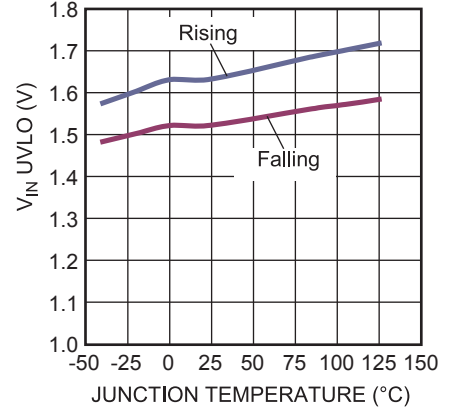
**Linear Charge Current vs. Output Voltage**



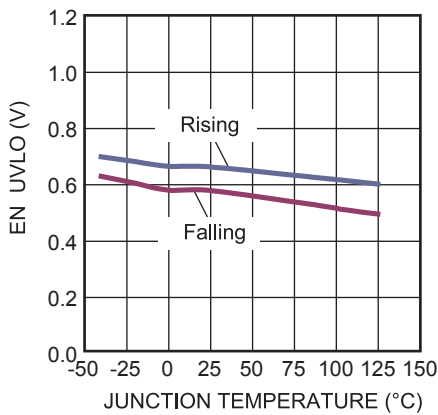
**Boost Current Limit vs. Duty Cycle**



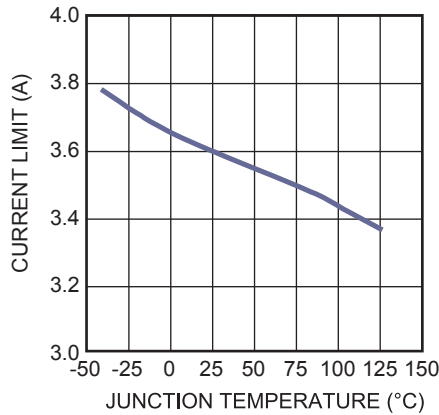
**$V_{IN}$  UVLO vs. Junction Temperature**



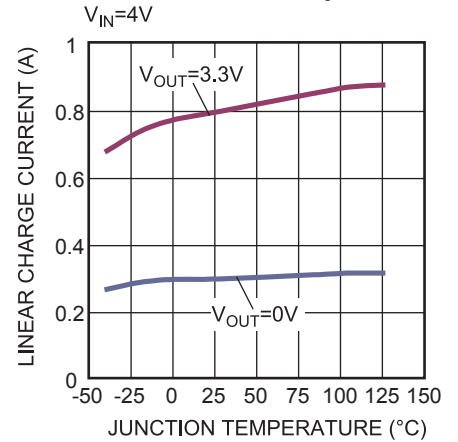
**EN UVLO vs. Junction Temperature**



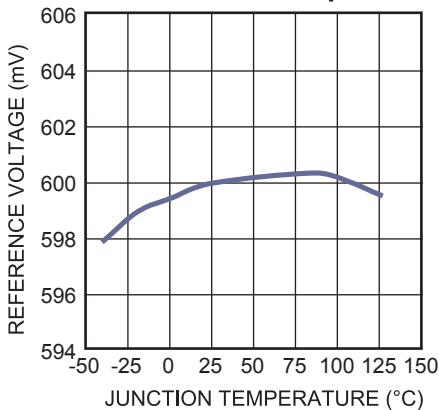
**Boost Current Limit vs. Junction Temperature**



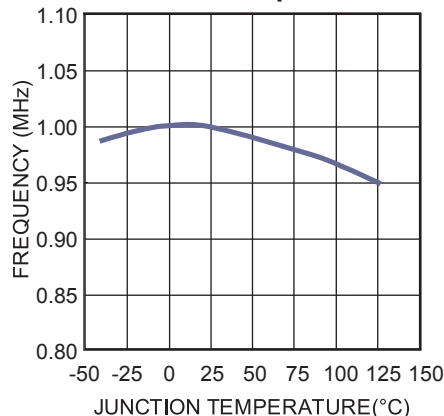
**Linear Charge Current vs. Junction Temperature**



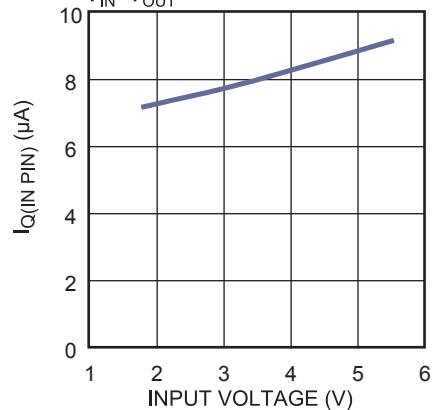
**Reference Voltage vs. Junction Temperature**

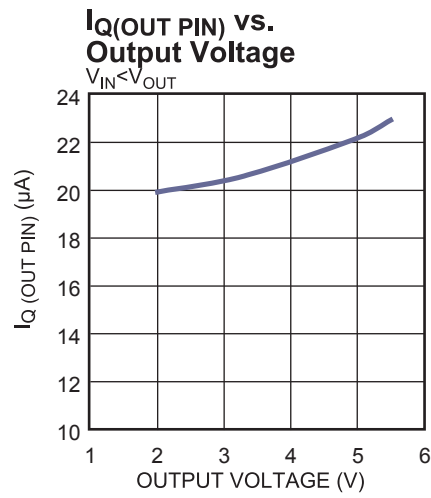


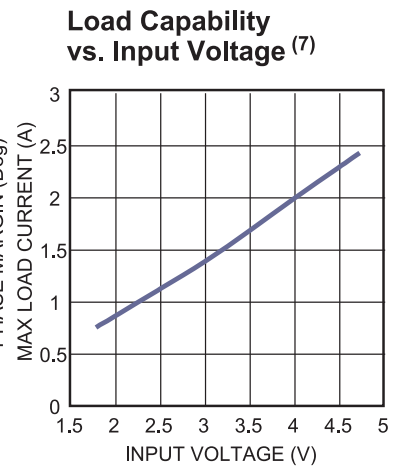
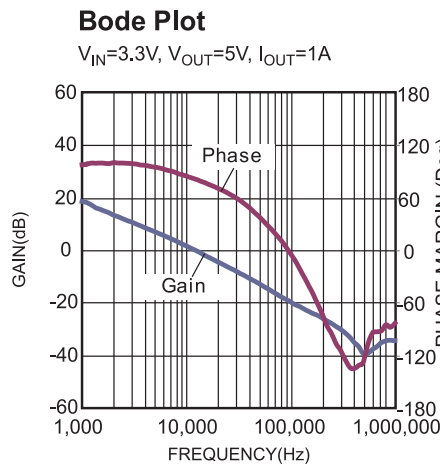
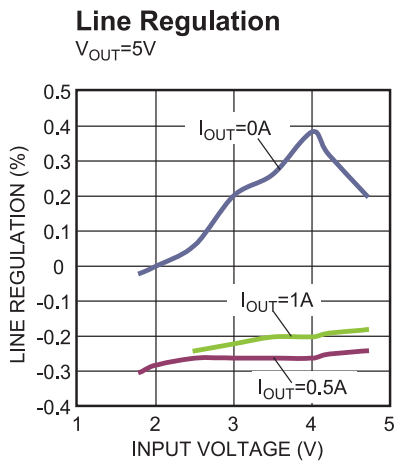
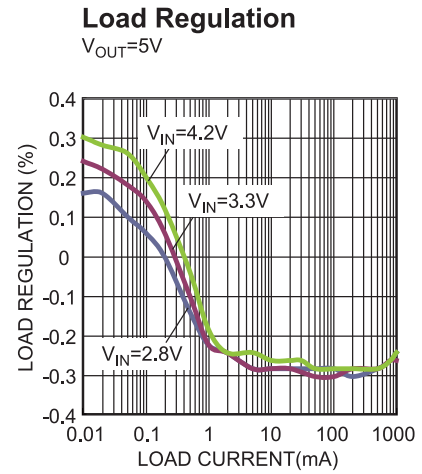
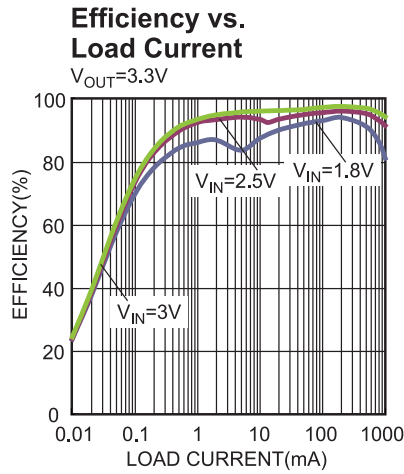
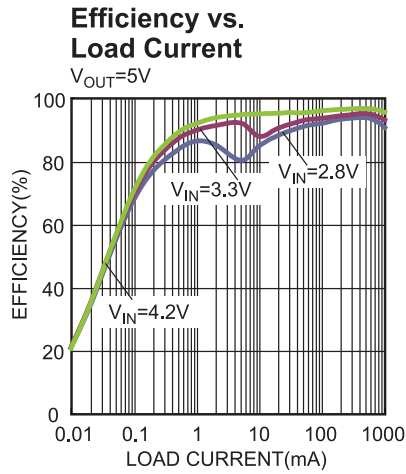
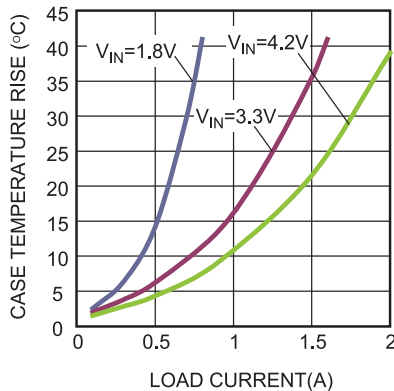
**Frequency vs. Junction Temperature**



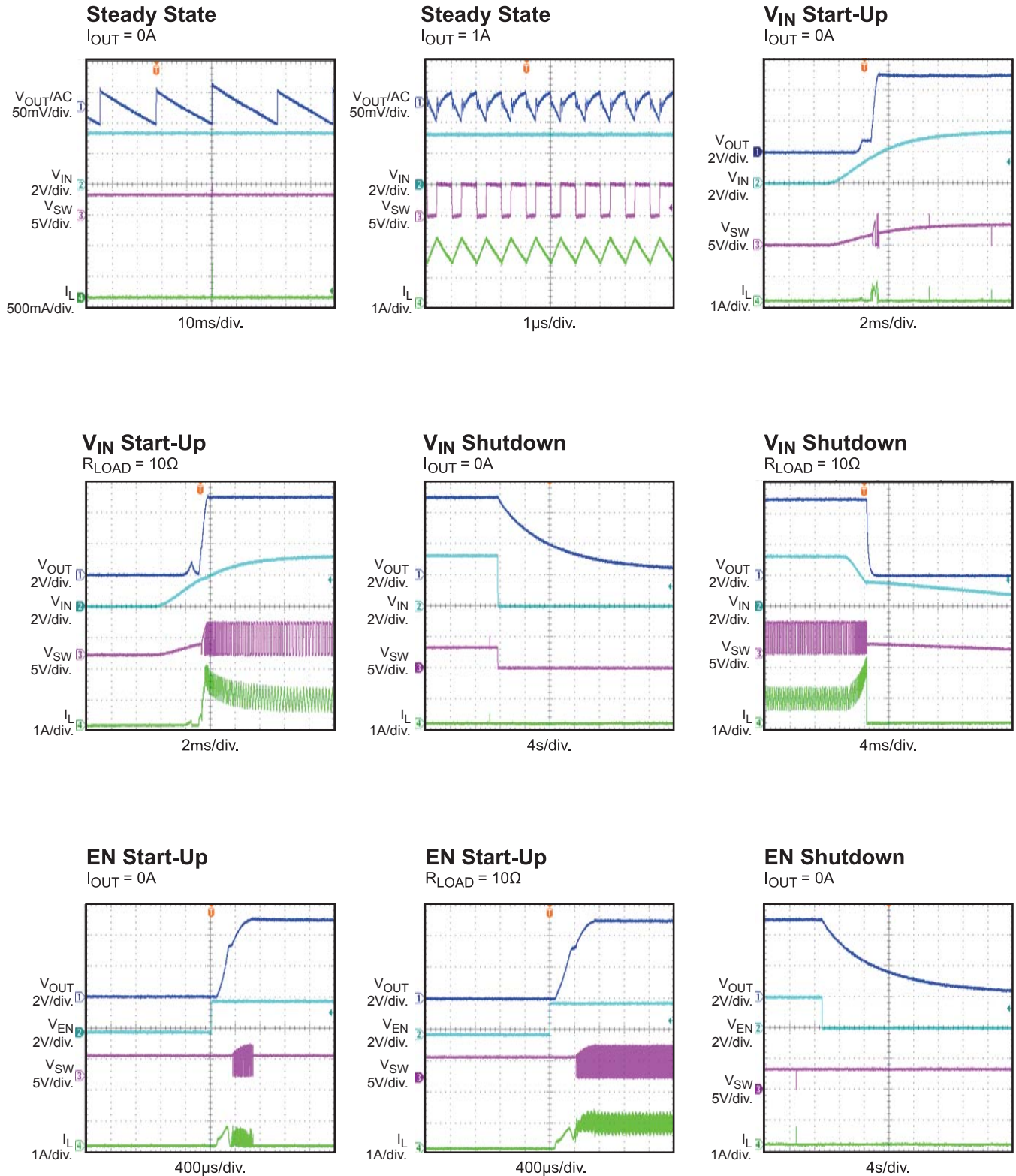
**$I_{Q(IN PIN)}$  vs. Input Voltage**



**TYPICAL PERFORMANCE CHARACTERISTICS** *(continued)* $V_{IN} = 3.3V$ ,  $V_{OUT} = 5V$ ,  $L = 1.5\mu H$ ,  $T_A = 25^\circ C$ , unless otherwise noted.

**TYPICAL PERFORMANCE CHARACTERISTICS (continued)**
 $V_{IN} = 3.3V$ ,  $V_{OUT} = 5V$ ,  $L = 1.5\mu H$ ,  $T_A = 25^\circ C$ , unless otherwise noted.

**Case Temperature Rise**

**NOTE:**

7) Tested with a 3A inductor peak current with the schematic in Figure 3. The maximum load current may decrease if the temperature rising is limited on the real application board.

**TYPICAL PERFORMANCE CHARACTERISTICS (continued)**
 $V_{IN} = 3.3V$ ,  $V_{OUT} = 5V$ ,  $L = 1.5\mu H$ ,  $T_A = 25^\circ C$ , unless otherwise noted.


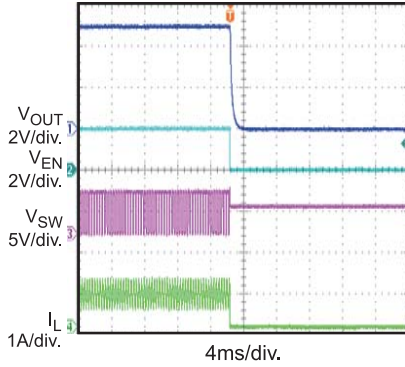


**TYPICAL PERFORMANCE CHARACTERISTICS** *(continued)*

$V_{IN} = 3.3V$ ,  $V_{OUT} = 5V$ ,  $L = 1.5\mu H$ ,  $T_A = 25^\circ C$ , unless otherwise noted.

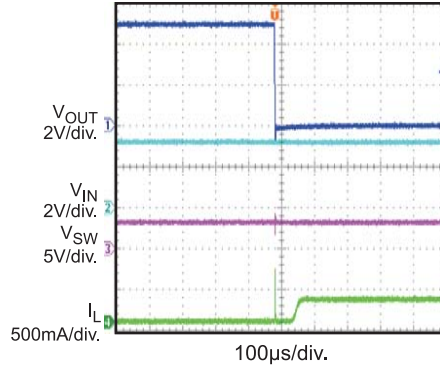
**EN Shutdown**

$R_{LOAD} = 10\Omega$



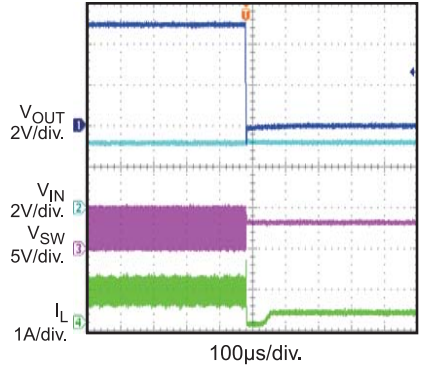
**SCP Entry**

$I_{OUT} = 0A$  to Short



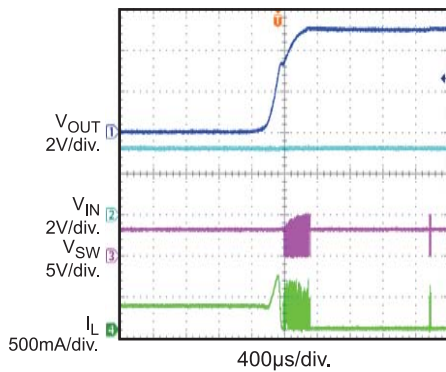
**SCP Entry**

$R_{LOAD} = 10\Omega$  to Short



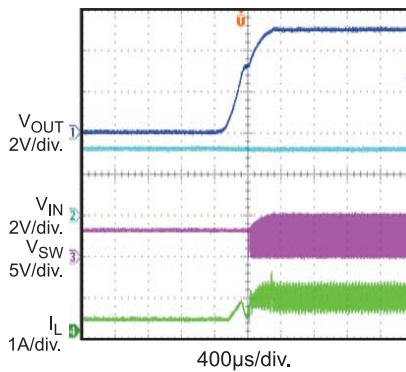
**SCP Recovery**

$I_{OUT} = \text{Short to } 0A$



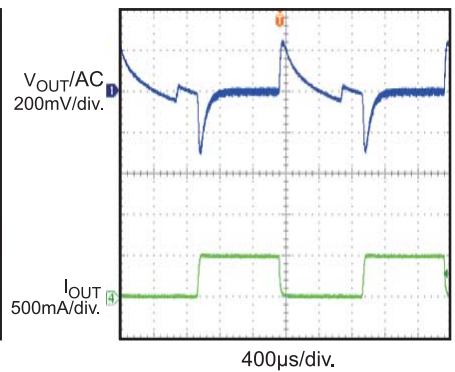
**SCP Recovery**

$R_{LOAD} = \text{Short to } 10\Omega$



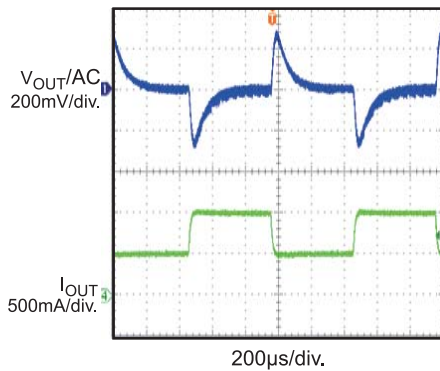
**Load Transient**

$I_{OUT} = 0A$  to 0.5A



**Load Transient**

$I_{OUT} = 0.5A$  to 1A



## PIN FUNCTIONS

Pin #	Name	Pin Function
1	IN	<b>Power supply input.</b> The start-up bias is derived from IN and must be bypassed locally. Once the OUT voltage exceeds the IN voltage, the bias power comes from OUT.
2	OUT	<b>Output.</b> OUT is the drain of the internal synchronous rectifier MOSFET. Bias power is derived from OUT when $V_{OUT}$ is higher than $V_{IN}$ . The PCB trace length from OUT to the output filter capacitor(s) should be as short and wide as possible. The output disconnect feature allows OUT to be disconnected completely from IN when EN is low.
3	SW	<b>Power switch output.</b> SW is the connection node of the internal low-side MOSFET and synchronous MOSFET. Connect the power inductor between SW and the input power. Keep the PCB trace length as short and wide as possible to reduce EMI and voltage spikes.
4	PGND	<b>Power ground.</b>
5	FTY	<b>Factory use only.</b> Leave FTY floating or connect it to ground in application.
6	AGND	<b>Analog ground.</b>
7	FB	<b>Feedback.</b> Connect to the tap of an external resistive voltage divider from the output to FB to set the output voltage.
8	EN	<b>Chip enable control input.</b> Set EN higher than 1.2V to turn on the regulator. Set EN lower than 0.4V to turn off the regulator.

FUNCTION DIAGRAM

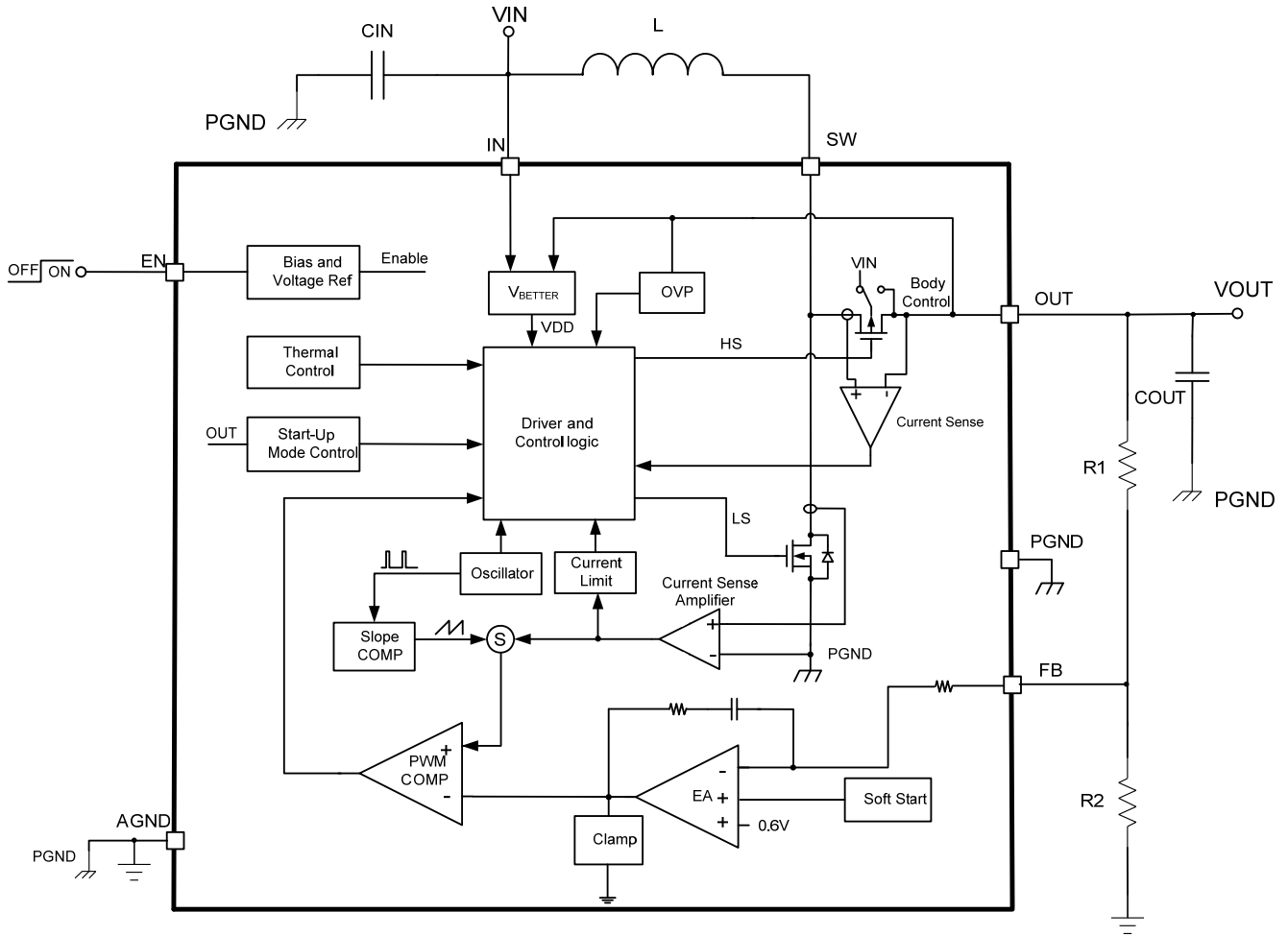


Figure 1: Functional Block Diagram

## OPERATION

The MP3414A is a 1MHz synchronous step-up converter in a compact TSOT23 package with true output disconnect. The device features a fixed-frequency, current-mode PWM control for good line and load regulation. Internal soft start and loop compensation simplify the design process and minimize external components. The combined internal low  $R_{DS(ON)}$  MOSFETs and frequency stretching allow the MP3414A to maintain high efficiency over a wide current load range.

### Start-Up

When enabled, the MP3414A starts up in linear charge mode. During the linear charge, the rectified PMOS turns on until the output voltage is charged close to  $V_{IN}$ . To avoid inrush current, the PMOS current is limited to about 0.3A (when  $V_{OUT}$  is 0V). The PMOS linear charge current limit is increased to about 0.8A while  $V_{OUT}$  rises to 3.3V (if  $V_{IN}$  is higher than 3.3V). This circuit helps limit the output current under short-circuit conditions. Once the output voltage reaches  $V_{IN}$ , the linear charging period elapses, and the device starts switching.  $V_{OUT}$  starts to rise under the control of the internal soft start (SS). In boost switching conditions, the current limit is 3.6A, typically.

When the output voltage is higher than  $V_{IN}$ , the MP3414A powers its internal circuits from  $V_{OUT}$  instead of  $V_{IN}$ . This allows strong driving capabilities and high efficiency, even if  $V_{IN}$  drops as low as 1.8V.

### Soft Start (SS)

The MP3414A provides a soft start (SS) by charging an internal capacitor with a current source. During the linear charge period, the SS signal keeps rising, following FB. Once the linear charge elapses, the voltage on the SS capacitor is charged and ramps up the reference voltage based on the internal fixed slew-rate. The SS capacitor is discharged completely during a commanded shutdown, thermal shutdown, or short circuit at the output.

### Device Enable (EN)

The device begins operating if EN is set higher than 1.2V. It enters shutdown mode if EN is lower than 0.4V. In shutdown mode, the regulator stops switching, all internal control

circuits switch off, and the output disconnects from the input completely.

### Power-Save Mode (PSM)

The MP3414A enters power-save mode (PSM) automatically when the load decreases. It switches back to PWM mode when the load increases. In PSM, the converter stretches the frequency down to save switching and driver losses. In addition, the switch frequency is stretched down too when the input voltage is close to the output voltage (which triggers the minimum on-time if kept at a 1MHz frequency). This helps decrease the output ripple by avoiding group-pulse mode. Under a very light-load condition, the MP3414A continues to run in group-pulse mode to regulate the output voltage and save more power.

### Error Amplifier (EA)

The error amplifier (EA) is an internally compensated amplifier. The EA compares the internal 0.6V reference voltage against  $V_{FB}$  to generate an EA signal, which in turn controls  $V_{OUT}$ . The output voltage of the MP3414A is adjusted via FB by an external resistor divider. See Equation (1):

$$V_{OUT} = 0.6V \times \left(1 + \frac{R1}{R2}\right) \quad (1)$$

Setting a high value for R1 and R2 achieves a low quiescent current. However, a resistance set too high will be sensitive to noise and lead to a low loop bandwidth. Set the R1 value between 499k $\Omega$  to 1M $\Omega$  for good leakage, stability and transient balance.

### Current Sensing

In a linear charge condition, the high-side PMOS current is sensed and compared with the current limit threshold. The compared output manages the linear charge current.

In a boost switching condition, lossless current sensing converts the NMOS switch current signal to a voltage that is summed with the internal slope compensation. The summed signal is compared with the EA output to provide a peak current control command for the PWM. The peak switch current is limited to approximately 3.6A. The switch current signal is

blanked for 60ns internally to enhance noise immunity.

### **Output Disconnect**

The MP3414A is designed to allow a true output disconnect by eliminating body diode conduction of the internal PMOS rectifier. This allows  $V_{OUT}$  to reach 0V during shutdown, drawing zero current from the input source.

This also allows for inrush current limiting at start-up, which minimizes the surge current seen by the input supply. To obtain the advantages of the output disconnect, there must NOT be an external Schottky diode connected between SW and  $V_{OUT}$ .

### **Overload (OLP) and Short-Circuit Protection (SCP)**

When an overload or a short circuit occurs, the output voltage drops. If  $V_{OUT}$  drops below  $V_{IN}$  (0.3V), the MP3414A stops for about 50 $\mu$ s and then runs in a linear charge mode at start-up. If the overload or short circuit is removed, the MP3414A restarts automatically under SS control.

### **Over-Voltage Protection (OVP)**

If the voltage on  $V_{OUT}$  is higher than the typical 6V threshold, the boost switching stops. After the output drops to about 5.7V, the switching recovers automatically. This protects the internal power MOSFET from over-voltage stress.

### **Thermal Shutdown (TSD)**

The device has an internal temperature monitor. If the die temperature exceeds 155°C, the converter turns off. Once the temperature drops below 130°C, the converter restarts.

## APPLICATION INFORMATION

### COMPONENT SELECTION

#### Input Capacitor Selection

Low equivalent series resistance (ESR) input capacitors reduce input switching noise and reduce the peak current drawn from the battery. Ceramic capacitors are recommended for input decoupling and should be placed as close to the device as possible. A ceramic capacitor larger than 10 $\mu$ F is recommended to limit the  $V_{IN}$  ripple.

#### Output Capacitor Selection

To ensure stability over the full operating range, the output capacitor requires a minimum capacitance value of 22 $\mu$ F at the programmed output voltage. A higher capacitance value may be required to lower the output and transient ripple. Low ESR capacitors such as X5R or X7R type are recommended. Supposing the ESR is zero, use Equation 2 to calculate the minimum output capacitor to support the ripple in the PWM mode:

$$C_o \geq \frac{I_o \times (V_{OUT(MAX)} - V_{IN(MIN)})}{f_s \times V_{OUT(MAX)} \times \Delta V} \quad (2)$$

$V_{OUT(MAX)}$  = Maximum output voltage

$V_{IN(MIN)}$  = Minimum input voltage

$I_o$  = Output current

$f_s$  = Switching frequency

$\Delta V$  = Acceptable output ripple

A 1 $\mu$ F ceramic capacitor is recommended between  $V_{OUT}$  and PGND with a short loop. This reduces spikes on the SW node and improves EMI performance.

#### Inductor Selection

The MP3414A utilizes small surface mounted chip inductors due to its 1MHz switching frequency. Inductor values between 1 $\mu$ H and 2.2 $\mu$ H are suitable for most applications. Larger values of inductance allow for slightly greater output current capabilities by reducing the inductor ripple current. However, larger value inductances will increase the component size. The minimum inductance value is given using Equation (3):

$$L \geq \frac{V_{IN(MIN)} \times (V_{OUT(MAX)} - V_{IN(MIN)})}{V_{OUT(MAX)} \times \Delta I_L \times f_s} \quad (3)$$

$\Delta I_L$  = Acceptable inductor current ripple

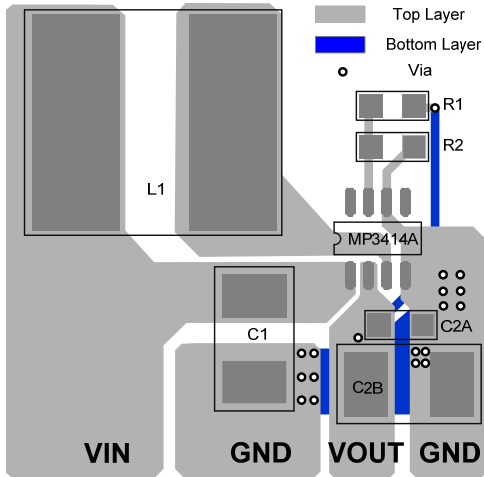
Typically, the inductor current ripple is set to 30% to 50% of the maximum inductor current. Maintain a low DCR (series resistance of the inductor) to reduce resistive power loss. The saturated current ( $I_{SAT}$ ) should be large enough to support the peak current.

#### PCB Layout Guidelines

Efficient PCB layout is critical for high-frequency switching power supplies. Poor layout can result in reduced performance, excessive EMI, resistive loss, system instability, and even over-voltage stress.

For best results, refer to Figure 2 and follow the guidelines below:

1. Place the output capacitor as close as possible to OUT with minimal distance to PGND. A small decoupling capacitor should be in parallel with the bulk output capacitor.
2. Place the small decoupling capacitor as close as possible to OUT and PGND. This is very important to reduce the spikes on SW and improve EMI performance.
3. Place the input capacitor and inductor as close as possible to IN and SW. The trace between the inductor and SW should be as wide and short as possible.
4. Place the feedback loop far away from all noise sources (such as SW). The feedback divider resistors should be as close as possible to FB and AGND.
5. Tie the ground return of the input/output capacitors as close as possible to PGND using a large copper GND area. Vias around GND are recommended to lower the die temperature.



**Figure 2: Recommended PCB Layout**

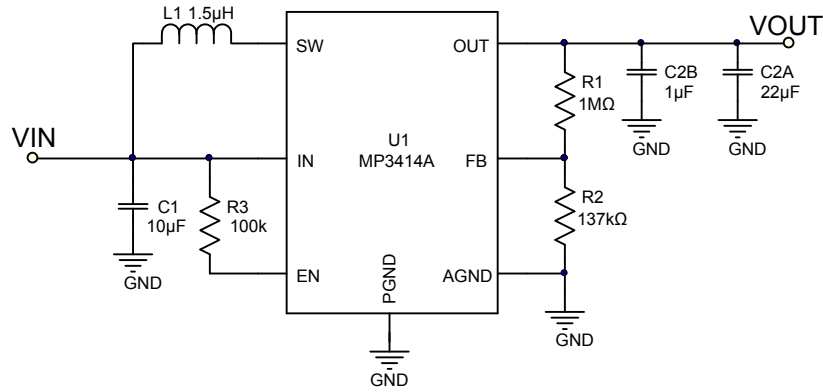
### Design Example

See Table 1 below for a design example following the application guidelines for the specifications below:

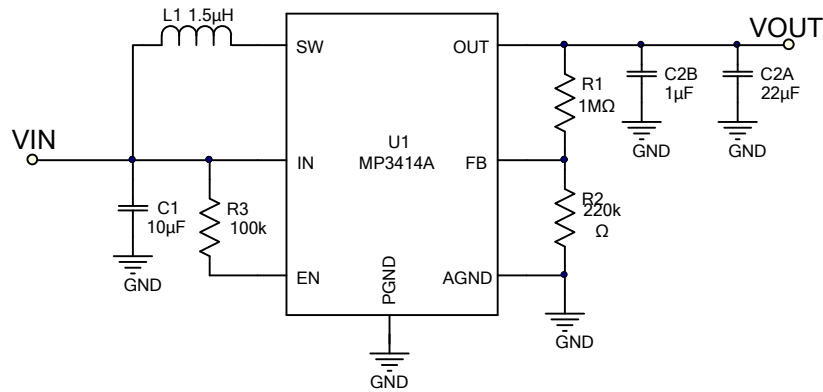
**Table 1: Design Example**

$V_{IN}$	2.8V-4.2V
$V_{OUT}$	5V
$I_{OUT}$	0A-1A

The typical application circuit for  $V_{OUT} = 5V$  in Figure 3 shows the detailed application schematic and the basis for the typical performance waveforms. For additional detailed device applications, please refer to the related evaluation board datasheet (EVB).

**TYPICAL APPLICATION CIRCUITS**


**Figure 3: Typical Boost Application Circuit,  $V_{IN} = 2.8V$  to  $4.2V$ ,  $V_{OUT} = 5V$ ,  $I_{OUT} = 0A-1A$**

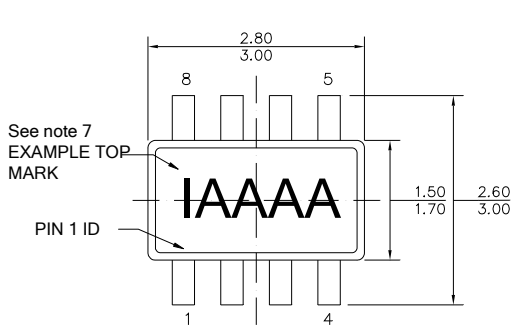


**Figure 4: Typical Boost Application Circuit,  $V_{IN} = 1.8V$  to  $3V$ ,  $V_{OUT} = 3.3V$ ,  $I_{OUT} = 0A-1A$**

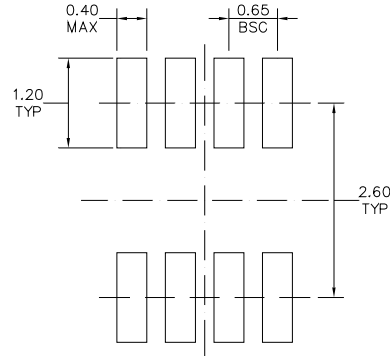


# PACKAGE INFORMATION

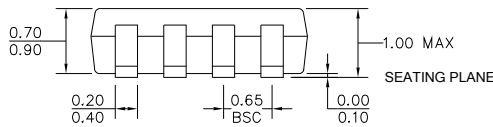
## TSOT23-8



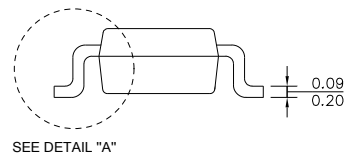
TOP VIEW



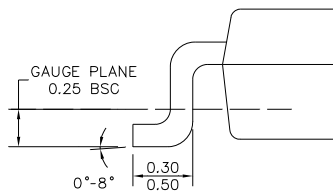
RECOMMENDED LAND PATTERN



FRONT VIEW



SIDE VIEW



DETAIL "A"

**NOTE:**

- 1) ALL DIMENSIONS ARE IN MILLIMETERS.
- 2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH, PROTRUSION OR GATE BURR.
- 3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION.
- 4) LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.10 MILLIMETERS MAX.
- 5) JEDEC REFERENCE IS MO-193, VARIATION BA.
- 6) DRAWING IS NOT TO SCALE.
- 7) PIN 1 IS LOWER LEFT PIN WHEN READING TOP MARK FROM LEFT TO RIGHT, (SEE EXAMPLE TOP MARK).

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