MP7751

26V, 2x20W Stereo BTL Fix Frequency Class D Audio Amplifier

The Future of Analog IC Technology

DESCRIPTION

MP7751 is an analog input Class D Audio Amplifier which can drive stereo speakers in bridge-tied-load configuration. It is one of MPS' products of fully integrated audio amplifiers which dramatically reduce solution size by integrating the following:

240mΩ power MOSFETs

Startup / Shutdown pop elimination

Short circuit protection circuits

Advanced EMI performance

The MP7751 utilizes a stereo BTL structure capable of delivering 20W per channel into 8Ω speakers at 18V power supply. MPS Class D Audio Amplifiers exhibit the high fidelity of a Class AB amplifier at high efficiencies.

The MP7751 includes an internal circuit which allows the system automatic shutdown after the absence of the audio signal. This feature is used for energy-using products and for battery operated applications.

It also has an adjustable power limit function. The PLIMIT circuit sets a limit on the output peak-to-peak voltage. The limiting is done by limiting the duty cycle to fixed maximum value. This limit can be thought of as a "virtual" voltage rail which is lower than the supply connected to PVCC.

The MP7751 is available in TSSOP-28 EP package.

FEATURES

- 5V to 26V Operation from a Single Supply
- ±5A Peak Current Output
- Output Power:
  9.5W/channel at 12V, 8Ω Load, 10%THD
  15W/Channel at 16V, 8Ω Load, 10%THD
  20W/Channel at 18V, 8Ω Load, 10%THD
- 92% Efficiency with 8Ω Load, 10%THD, 1kHz, 12V Supply Voltage
- 240mΩ power MOSFETs
- Startup / Shutdown pop elimination
- Short circuit protection circuits
- Advanced EMI performance
- All Switches Current limited
- Internal Under Voltage Protection
- Internal Thermal Protection
- TSSOP-28 EP package
- Adjustable power limiter
- Automatic shutdown with zero input signal detect
- Fault Output Flag

APPLICATIONS

- TV
- DVD Receiver
- Active Speaker
- Home Theaters

All MPS parts are lead-free and adhere to the RoHS directive. For MPS green status, please visit MPS website under Products, Quality Assurance page.

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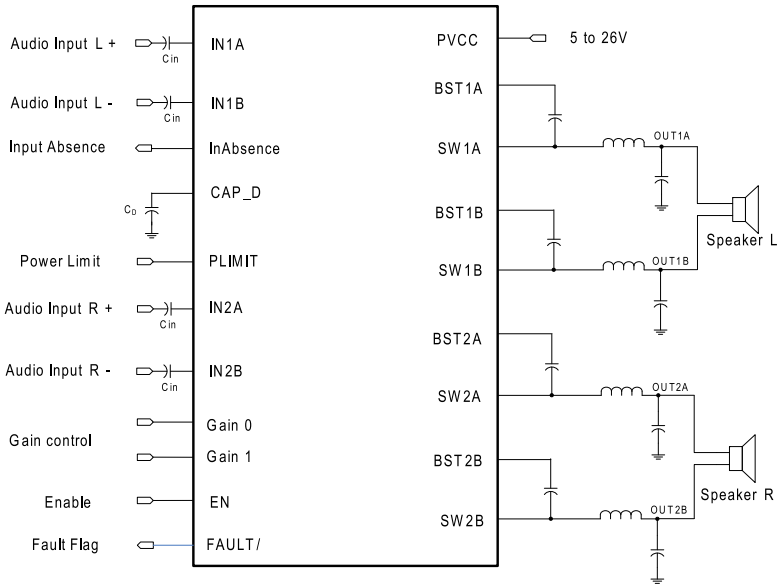
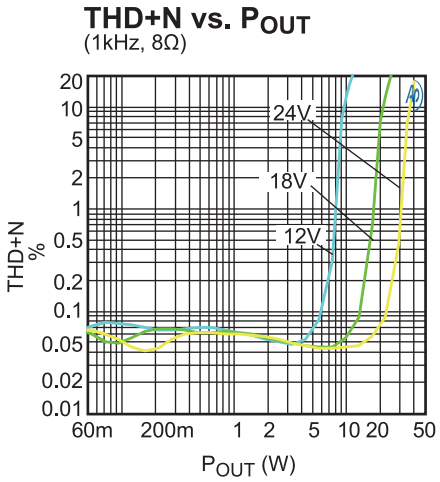
TYPICAL APPLICATION





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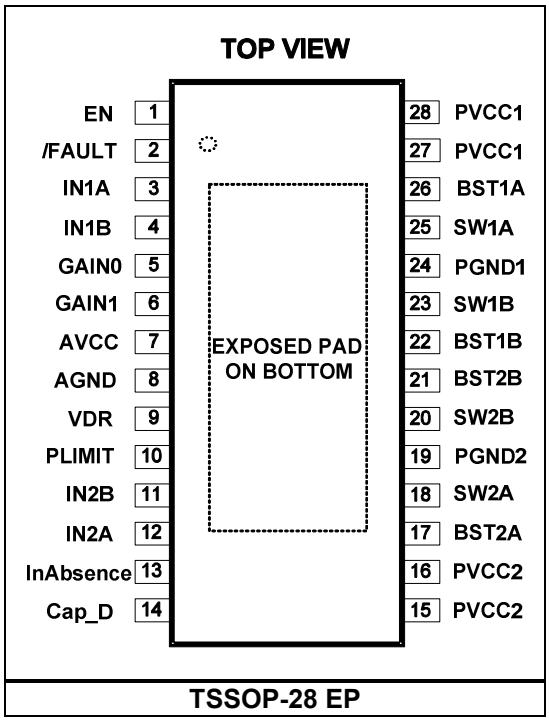
ORDERING INFORMATION

Part Number*	Package	Top Marking
MP7751GF	TSSOP-28 EP	MP7751

* For Tape & Reel, add suffix –Z (e.g. MP7751GF–Z)

PACKAGE REFERENCE



TSSOP-28 EP

ABSOLUTE MAXIMUM RATINGS (1)

Supply Voltage V_{CC} ..... –0.3V to +30V
V_{SW} ..... –1V to V_{CC} + 1V
V_{EN}, $V_{/FAULT}$, V_{GAIN}, $V_{InAbsence}$ – 0.3V to V_{CC} + 0.3V
BS Voltage V_{BST} ..... V_{SW} – 0.3V to V_{SW} + 6V
V_{PLIMIT} ..... – 0.3V to V_{AVCC} + 0.3V
V_{INXX} ..... – 0.3V to 6.5V
AGND to PGND ..... –0.3V to +0.3V
Continuous Power Dissipation (T_A = +25°C) (2) 3.9W
Junction Temperature ..... 150°C
Lead Temperature ..... 260°C
Storage Temperature ..... –65°C to +150°C

Recommended Operating Conditions (3)

Supply Voltage V_{IN} ..... 5V to 26V
Operating Junction Temp. (T_J) . -40°C to +125°C

Thermal Resistance (4)

	θ_{JA}	θ_{JC}	
TSSOP-28 EP	32	6	°C/W

Notes:

1) Exceeding these ratings may damage the device.
2) The maximum allowable power dissipation is a function of the maximum junction temperature T_J (MAX), the junction-to-ambient thermal resistance θ_{JA}, and the ambient temperature T_A. The maximum allowable continuous power dissipation at any ambient temperature is calculated by P_D (MAX) = (T_J (MAX)-T_A)/θ_{JA}. Exceeding the maximum allowable power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
3) The device is not guaranteed to function outside of its operating conditions.
4) Measured on JESD51-7, 4-layer PCB.

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ELECTRICAL CHARACTERISTICS (5,6)

V_{CC} = 24V, V_{EN} = 5V, T_j = -40°C to 125°C, unless otherwise noted.

Parameters	Symbol	Condition	Min	Typ	Max	Units
Standby Current	I_{QSTBY}	V_{EN} = 0V,NIN=PIN=Float		130	200	μA
Quiescent Current	I_Q	V_{EN} = 5V, no load, no LC filter		20	40	mA
Output Offset Voltage	V_{OS}	V_I = 0 V, Gain = 36 dB, T_j = 25°C		20	65	mV
SW On Resistance	R_{dsON}	I_O = 500mA, T_j = 25°C		0.24		Ω
Short Circuit Current		Sourcing and Sinking, T_j = 25°C	4	5	6	A
Closed Loop Gain	G	GAIN0 = L, GAIN1 = L	19	20	21	dB
		GAIN0 = H, GAIN1 = L	25	26	27	
		GAIN0 = L, GAIN1 = H	31	32	33	
		GAIN0 = H, GAIN1 = H	35	36	37	
EN Enable Threshold Voltage		V_{EN} Rising		1.3	2.0	V
		V_{EN} Falling	0.4	0.9		V
EN Enable Input Current		V_{EN} = 5V		12	25	μA
Under Voltage Protection		V_{UVP} Rising		4.6	5	V
		V_{UVP} Falling	4	4.3		V
AVCC Operating Voltage			5	5.5	6	V
VDR Operating Voltage			5	5.5	6	V
$V_{INN/INP}$ Common Mode Voltage			2.3	2.5	2.7	V
GAIN0/GAIN1 Threshold		V_{GAIN} Rising		1.6	2	V
		V_{GAIN} Falling	0.6	1.1		V
Turn-on Time	t_{ON}			13		ms
Turn-off Time	t_{OFF}			0.2		us
Switching frequency			260	325	360	kHz
Input signal absence sensitivity			2	5	8	mV
Thermal Shutdown Trip Point		T_J Rising		150		°C
Thermal Shutdown Hysteresis				20		°C

Note:

5) The device is not guaranteed to function outside its operating rating.
6) Electrical Characteristics are for the IC only with no external components except bypass capacitors.

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OPERATING SPECIFICATIONS (7)

Circuit of figure 5, V_{CC} = 24V, Gain=20dB, V_{EN} = 5V, R_{LOAD} = 8Ω, T_A = +25°C, unless otherwise noted.

Parameters	Symbol	Condition		Min	Typ	Max	Units
Power Output		f = 1kHz, THD+N = 10%, V_{CC} = 24V			36		W
		f = 1kHz, THD+N = 10%, V_{CC} = 18V			20		
		f = 1kHz, THD+N = 10%, V_{CC} = 12V			9.5		
THD+ Noise		P_{OUT} = 5W, f = 1kHz, V_{CC} = 12V			0.08		%
		P_{OUT} = 18W, f = 1kHz, V_{CC} = 24V			0.08		%
Efficiency		P_{OUT} = 9.5W + 9.5W, THD+N = 10%, V_{CC} = 12 V, 1kHz, R_{LOAD} = 8Ω			92		%
Deadtime		I_O=0.5A			28		nS
Cross Talk		V_O = 1 Vrms, f = 217Hz			-100		dB
Noise Floor		A-Weighted, 22 Hz to 22 kHz			120		μV
Signal-to-noise ratio		f = 1kHz, THD+N = 1%, A-Weighted			-96		dB
Power Supply Rejection		V_{RIPPLE}=200mV_{PP}, Inputs ac-coupled to AGND	f = 1kHz		-60		dB
			f = 217Hz		-60		dB

Note:

7) Operating Specifications are for the IC in Typical Application circuit. Not production tested.

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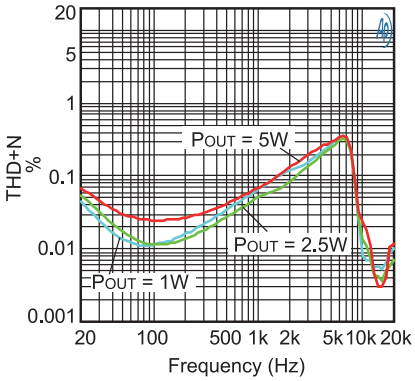
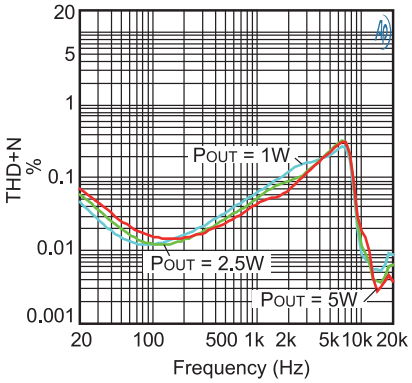
TYPICAL PERFORMANCE CHARACTERISTICS

V_{CC} = 12V, GAIN = 20dB, f = 1kHz, T_A = 25°C, using MP7751 EVB, unless otherwise noted.

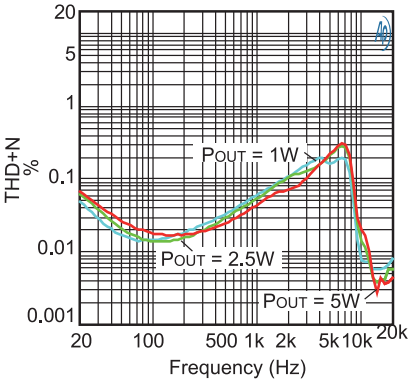
THD+N vs. Frequency
(12V, 8Ω)



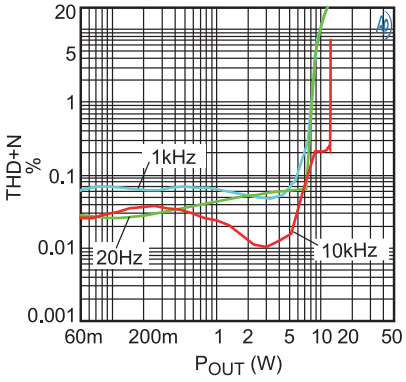
THD+N vs. Frequency
(18V, 8Ω)



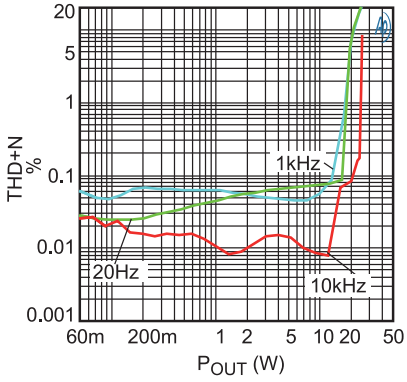
THD+N vs. Frequency
(24V, 8Ω)



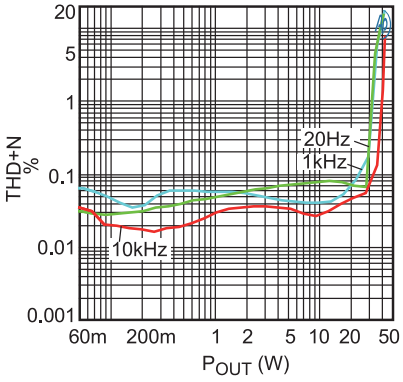
THD+N vs. POUT
(12V, 8Ω)



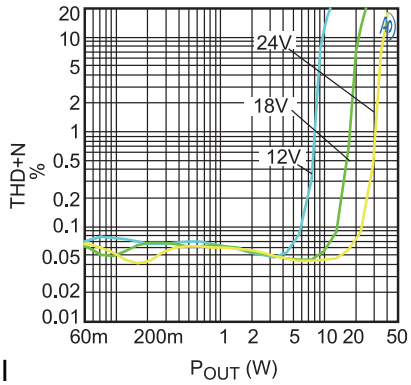
THD+N vs. POUT
(18V, 8Ω)



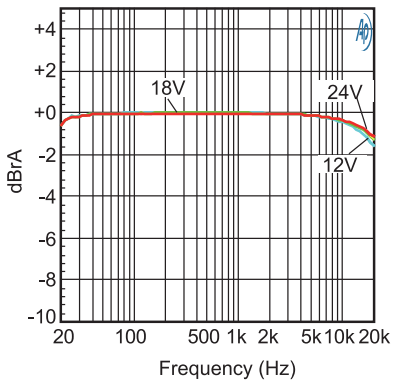
THD+N vs. POUT
(24V, 8Ω)



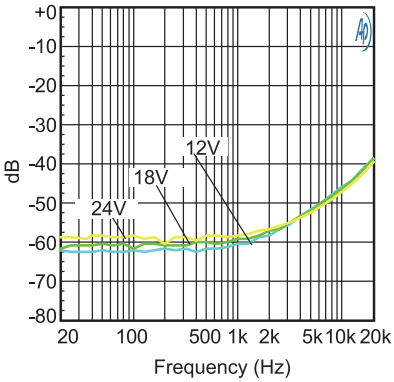
THD+N vs. POUT
(1kHz, 8Ω)



Frequency Response
(8Ω, 1W)



PSRR Test
(Gain=20dB, V_{AC_RIPPLE}=300mV_{PP})



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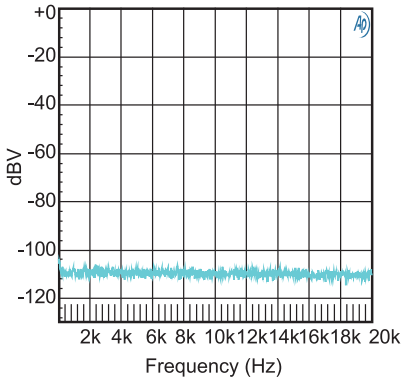
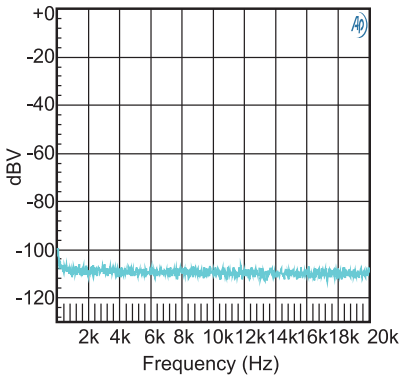
TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

V_{CC} = 12V, GAIN = 20dB, f = 1kHz, T_A = 25°C, using MP7751 EVB, unless otherwise noted.

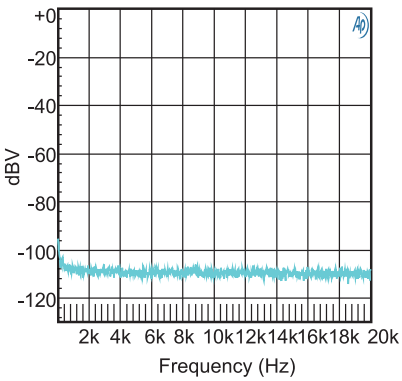
FFT Noise Floor Test
(12V, 8Ω)



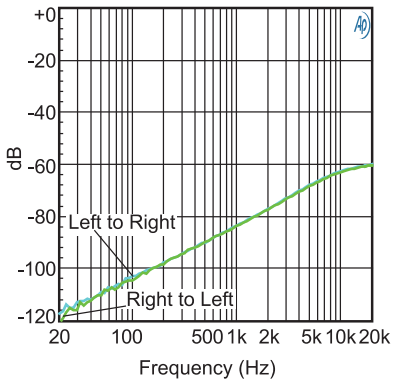
FFT Noise Floor Test
(18V, 8Ω)



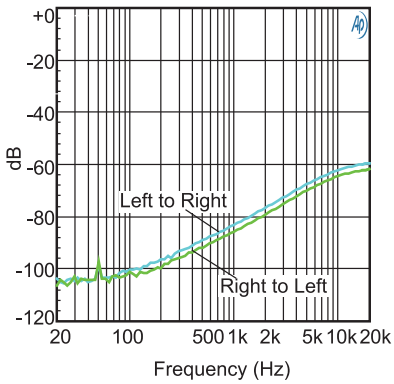
FFT Noise Floor Test
(24V, 8Ω)



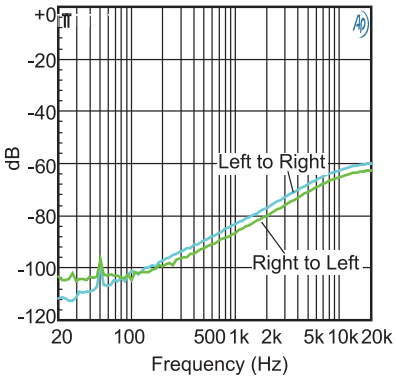
Cross Talk
(12V, 8Ω, P_{OUT}=5W)



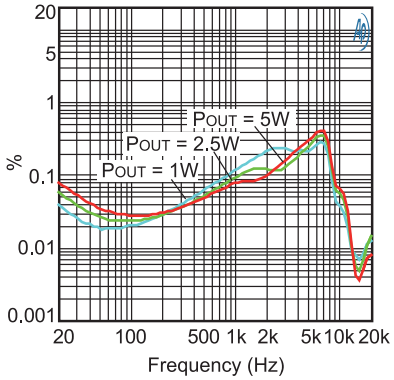
Cross Talk
(18V, 8Ω, P_{OUT}=5W)



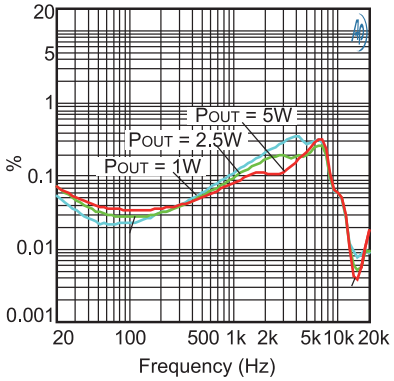
Cross Talk
(24V, 8Ω, P_{OUT}=5W)



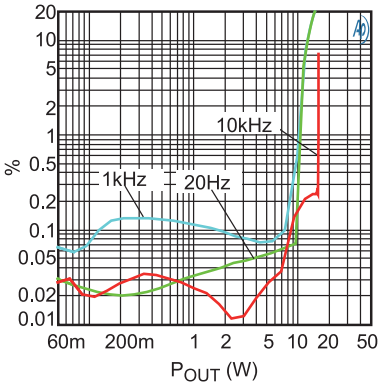
THD+N vs. Frequency
(12V, 6Ω)



THD+N vs. Frequency
(18V, 6Ω)



THD+N vs. POUT
(12V, 6Ω)



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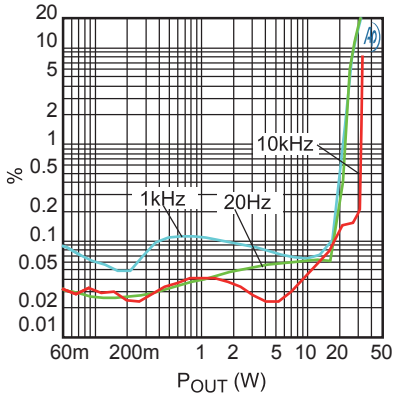
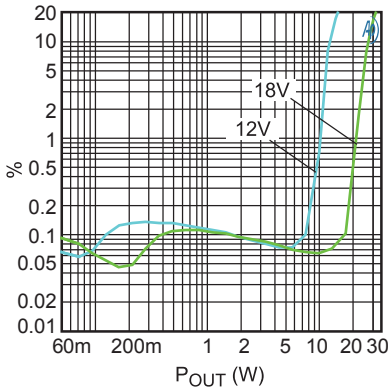
TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

V_{CC} = 12V, GAIN = 20dB, f = 1kHz, T_A = 25°C, using MP7751 EVB, unless otherwise noted.

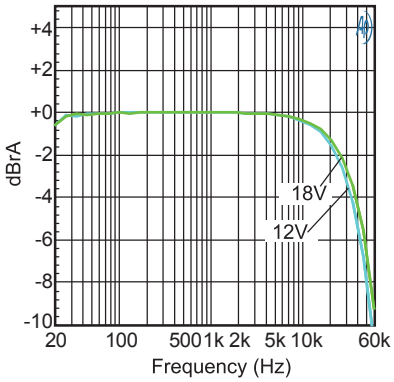
THD+N vs. P_{OUT}
(18V, 6Ω)



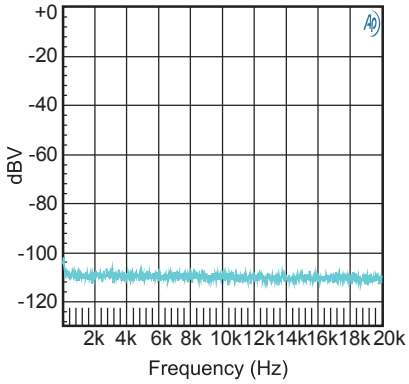
THD+N vs. P_{OUT}
(1kHz, 6Ω)



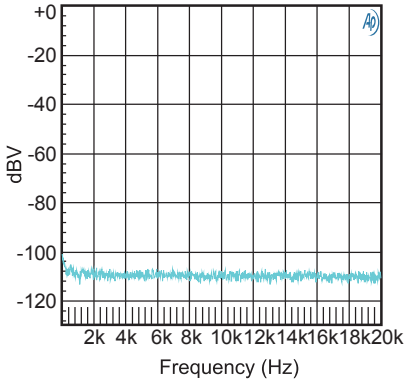
Frequency Response
(6Ω, 1W)



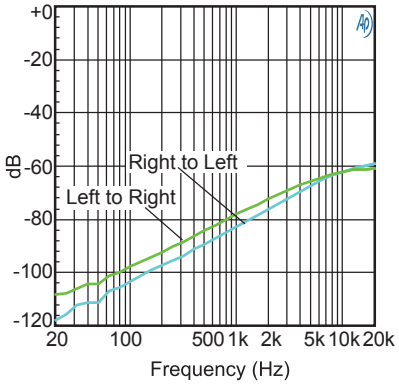
FFT Noise Floor Test
(12V, 6Ω)



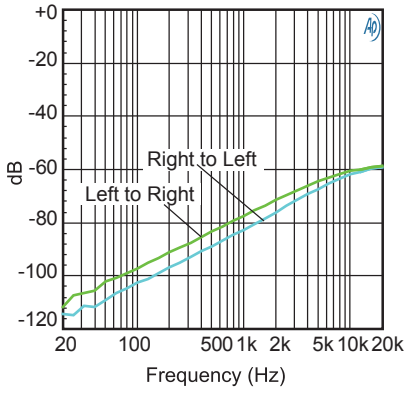
FFT Noise Floor Test
(18V, 6Ω)



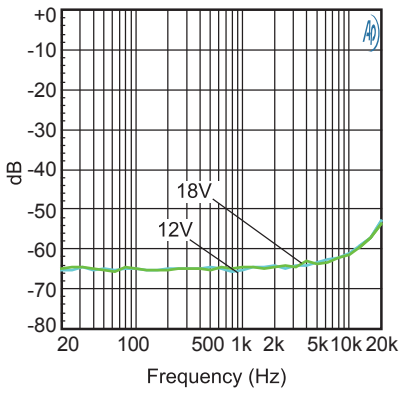
Cross Talk Test
(12V, 6Ω, P_{OUT}=5W)



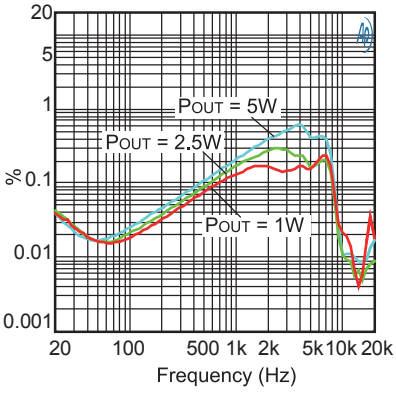
Cross Talk Test
(18V, 6Ω, P_{OUT}=5W)



PSRR Test
(Gain=20dB, V_{AC_RIPPLE}=300mV_{PP})



THD+N vs. Frequency
(12V, 4Ω)



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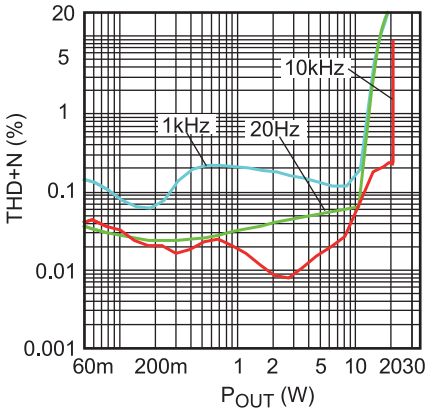
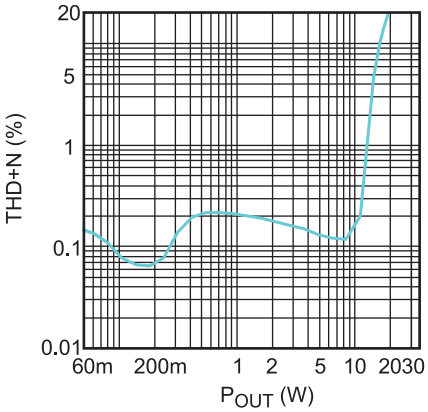
TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

V_{CC} = 12V, GAIN = 20dB, f = 1kHz, T_A = 25°C, using MP7751 EVB, unless otherwise noted.

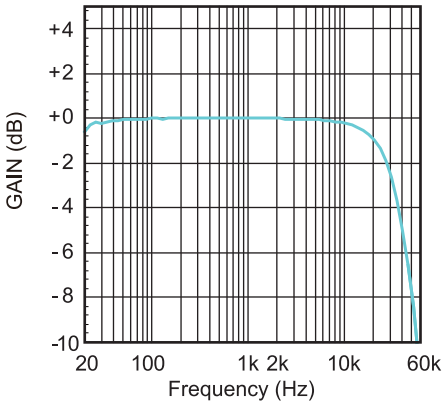
THD+N vs. P_{OUT}
(12V, 4Ω)



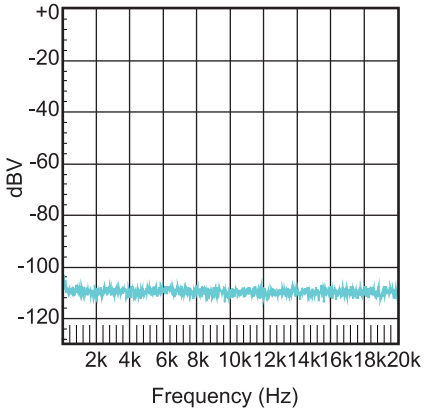
THD+N vs. P_{OUT}
(12V, 4Ω, 1kHz)



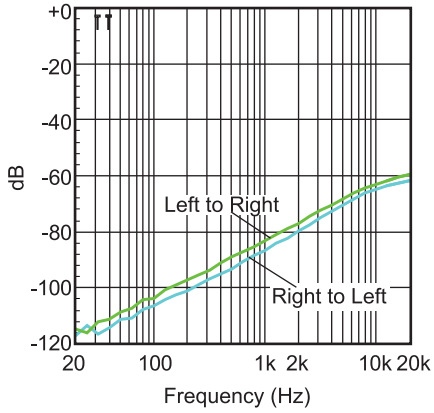
Frequency Response
(12V, 4Ω, 1W)



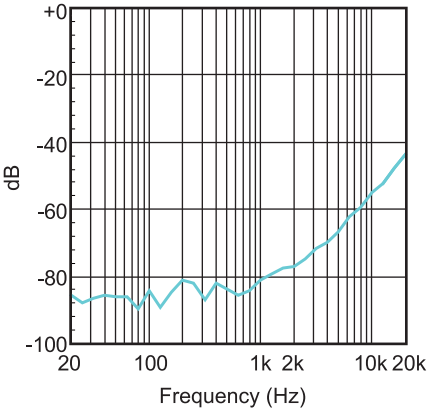
FFT Noise Floor Test
(12V, 4Ω)



Cross Talk
(12V, 4Ω, P_{OUT}=5W)



PSRR Test
(Gain=20dB, V_{AC_RIPPLE}=300mV_{PP}, C_{BYPASS}=2.2μF)



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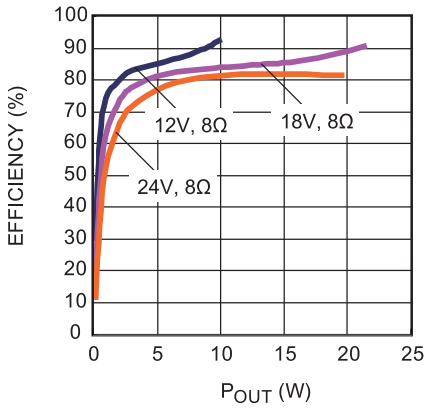
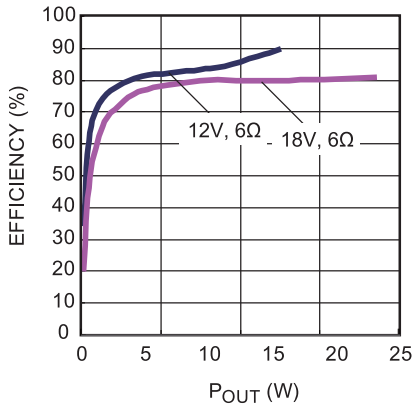
TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

V_{CC} = 12V, GAIN = 20dB, f = 1kHz, Stereo, T_A = 25°C, using MP7751 EVB, unless otherwise noted.

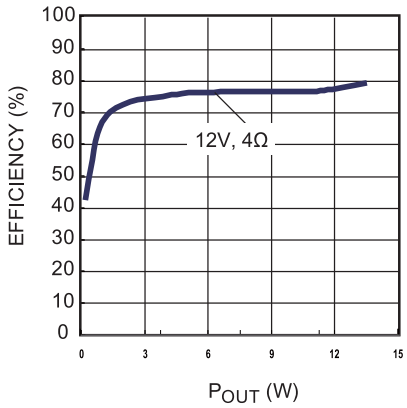
P_{OUT} vs. Efficiency



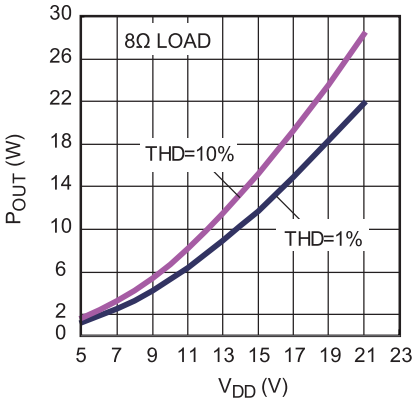
P_{OUT} vs. Efficiency



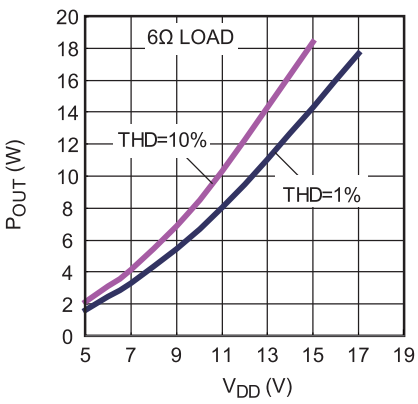
P_{OUT} vs. Efficiency



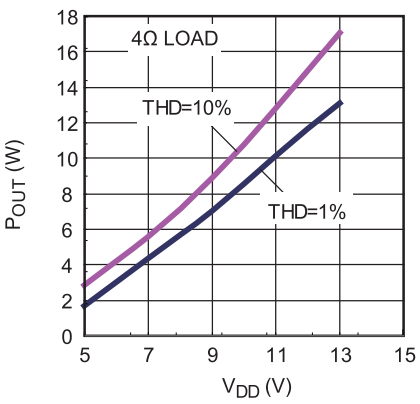
V_{DD} vs. P_{OUT}



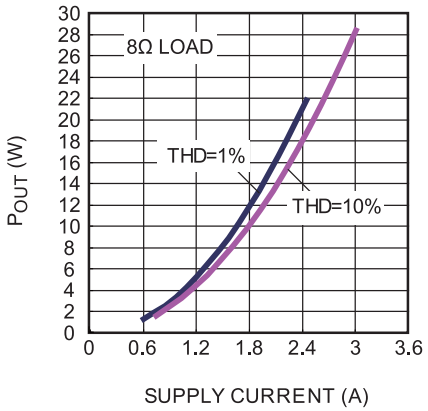
V_{DD} vs. P_{OUT}



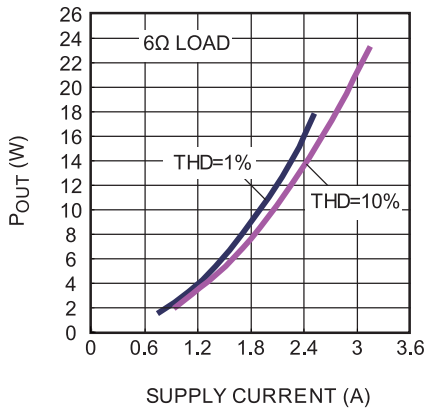
V_{DD} vs. P_{OUT}



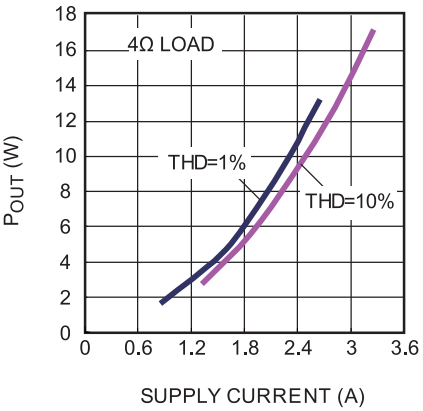
Supply Current vs. P_{OUT}



Supply Current vs. P_{OUT}



Supply Current vs. P_{OUT}



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PIN FUNCTIONS

Pin #	Name	Description
1	EN	Enable input. Drive EN high to turn on the Amplifier 1A/1B/2A/2B, low to turn them off.
2	/FAULT	Fault Output. A low output at FAULT indicates that the IC has detected an over temperature or over current condition. This output is open drain.
3	IN1A	Positive audio input for channel 1. Biased at 2.5V.
4	IN1B	Negative audio input for channel 1. Biased at 2.5V.
5	GAIN0	Gain selection bit.
6	GAIN1	Gain selection bit.
7	AVCC	Internal analog reference, 5.5V, need connect a bypass capacitor from AVCC to AGND.
8	AGND	Analog ground.
9	VDR	Gate Drive Supply Bypass. VDR powers the internal circuitry, internal MOSFET gate drive. Bypass VDR to AGND with a 0.1μF to 10μF capacitor.
10	PLIMIT	Power limit and anti-clipping feature control. Connect a resistor divider from AVCC to GND to set power limit. Connect directly to AVCC for no power limit.
11	IN2B	Negative audio input for channel 2. Biased at 2.5V.
12	IN2A	Positive audio input for channel 2. Biased at 2.5V.
13	InAbsence	Open drain output used to report the input signal absence.
14	Cap_D	Delay Time control for input signal absence report function. This holding time can be adjusted with external capacitor. Connect this pin to AGND to disable automatic shutdown with zero signal input function.
15, 16	PVCC2	Power supply input for channel 2. Bypass PVCC2 to PGND2 with a 1μF X7R capacitor (in addition to the main bulk capacitor), placed close to the PVCC2 and PGND2 pins.
17	BST2A	High-side MOSFET bootstrap input for Amplifier 2A. A capacitor from BST2A to SW2A supplies the gate drive current to the internal high-side MOSFET.
18	SW2A	Switched power output for Amplifier 2A (the positive output of channel 2).
19	PGND2	Power ground for Amplifier 2A/2B.
20	SW2B	Switched power output for Amplifier 2B (the negative output of channel 2).
21	BST2B	High-side MOSFET bootstrap input for Amplifier 2B. A capacitor from BST2B to SW2B supplies the gate drive current to the internal high-side MOSFET.
22	BST1B	High-side MOSFET bootstrap input for Amplifier 1B. A capacitor from BST1B to SW1B supplies the gate drive current to the internal high-side MOSFET.
23	SW1B	Switched power output for Amplifier 1B (the negative output of channel 1).
24	PGND1	Power ground for Amplifier 1A/1B.
25	SW1A	Switched power output for Amplifier 1A (the positive output of channel 1).
26	BST1A	High-side MOSFET bootstrap input for Amplifier 1A. A capacitor from BST1A to SW1A supplies the gate drive current to the internal high-side MOSFET.
27, 28	PVCC1	Power supply input for channel 1. Bypass PVCC1 to PGND1 with a 1μF X7R capacitor (in addition to the main bulk capacitor), placed close to the PVCC1 and PGND1 pins.

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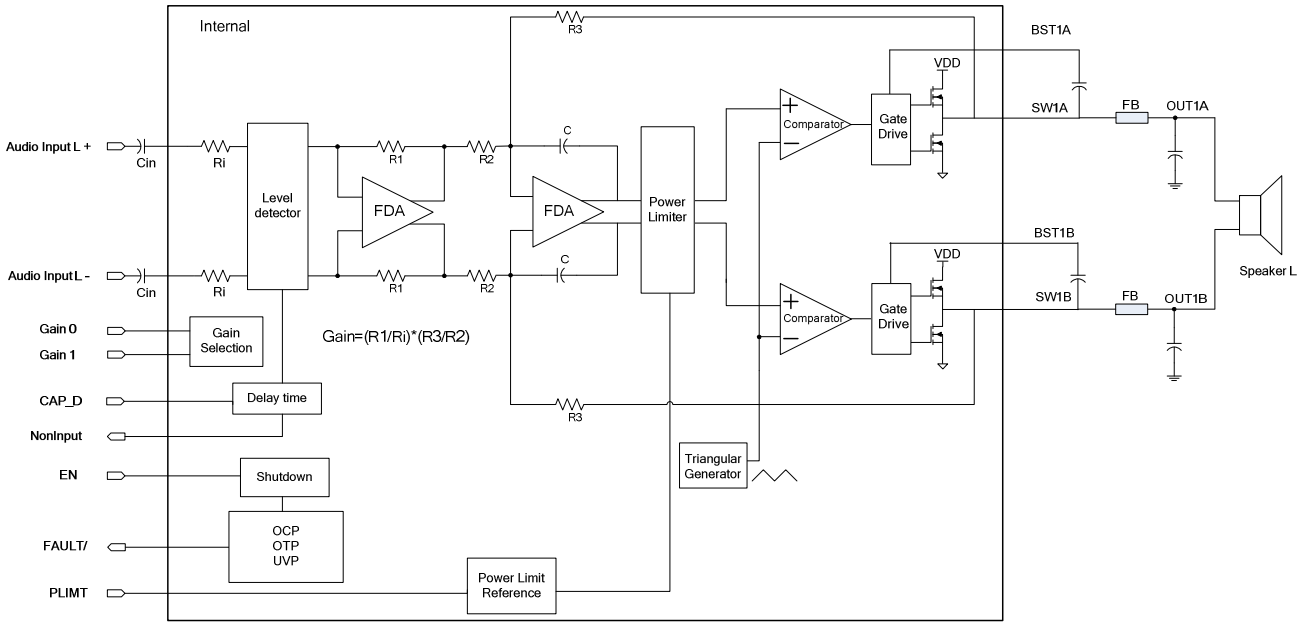
FUNCTIONAL BLOCK DIAGRAM



Functional Block Diagram (only one channel)

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OPERATION

The MP7751 is a fully integrated Class D stereo BTL audio amplifier. Because of the switching Class D output stage, power dissipation in the amplifier is drastically reduced when compared to Class A, B or A/B amplifiers while maintaining high fidelity and low distortion.

The amplifier has fully differential outputs and inputs. The differential input is useful to minimize the common-mode noise (any noise that appears on both input lines of the channel). This device can still be used with a single-ended input.

The MP7751 includes eight high-power MOSFETs wherein for each half-bridge channel the output driver stage uses two N-Channel MOSFETs to deliver the pulses to the LC output filter which in turn drives the load. To fully enhance the high-side MOSFET, the gate is driven to a voltage higher than the source by the bootstrap capacitor between OUTxx and BSTxx pins. While the output is driven low, the bootstrap capacitor is charged from power supply through an internal circuit. The gate of the high-side MOSFET is driven high from the voltage at Bootstrap Supply, forcing the MOSFET gate to a voltage higher than power supply voltage and allowing the MOSFET to fully turn on, reducing power loss in the amplifier.

The gain of the MP7751 is set by the input terminals, GAIN0 and GAIN1. The actual gain settings are controlled by ratios of the input and feedback resistors

Enable Function

The MP7751 EN input is an active high enable control. To enable the MP7751, drive EN with a 2.0V or higher voltage. To disable the amplifier, drive it below 0.4V. While the MP7751 is disabled, the PVCC operating current is around 250μA and the output driver MOSFETs are turned off.

Input signal Absence detect

The MP7751 includes an internal circuit which allows the system automatic shutdown after the absence of the audio signal. This feature is used for energy-using products and for battery operated applications.

The MP7751 includes a delay circuit which allows the IC continues to hold the flag after the absence of the audio signal. This holding time can be adjusted with external capacitor.

1. The input absence flag will be high initially when power on. After device enabled, the internal circuit start to detect the input signal. MP7751 will then hold the output report and normal operation for a delay time which can be adjusted by the Capacitor value @ pin 14. Then MP7751 will turn off the all MOSFETs and pull low the input absence output, until the input signal detected again.

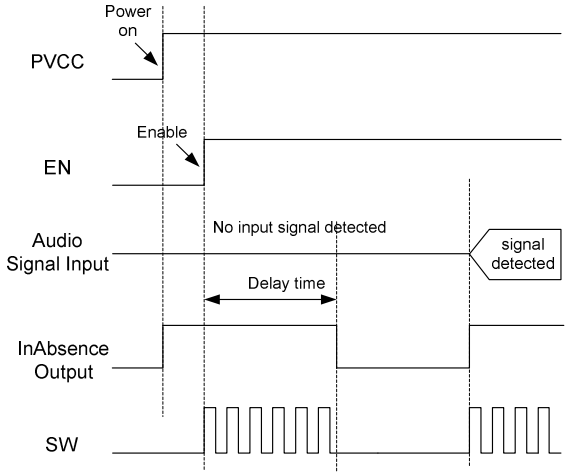

Figure 1a: enable on with no signal detected

2. The input absence flag output will be or maintain high when input signal is detected. The delay circuit will only be activated when the input signal absence. MP7751 will then hold the output report for a delay time which can be adjusted by the Capacitor value @ pin 14. Then MP7751 will turn off the all MOSFETs and pull low the input absence output, until the input signal detected again.

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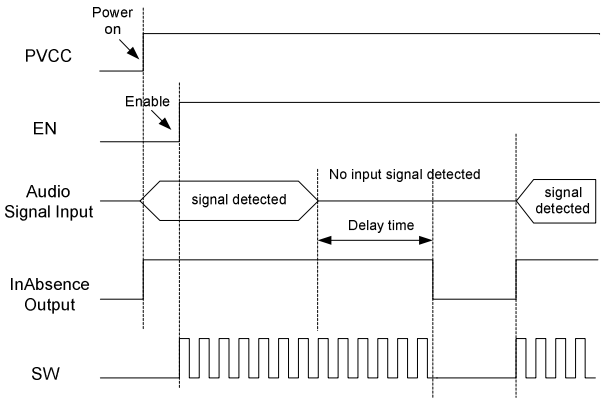

Figure 1b: enable on with audio signal present

Adjustable Power Limit

Power limit and anti-clipping feature control. The voltage at pin 10 can used to limit the power to levels below that which is possible based on the supply rail.
Connect a resistor divider from AVCC to GND to set power limit. Connect directly to AVCC for no power limit.

An external reference may also be used if tighter tolerance is required. Also add a 1μF capacitor from pin 10 to ground.

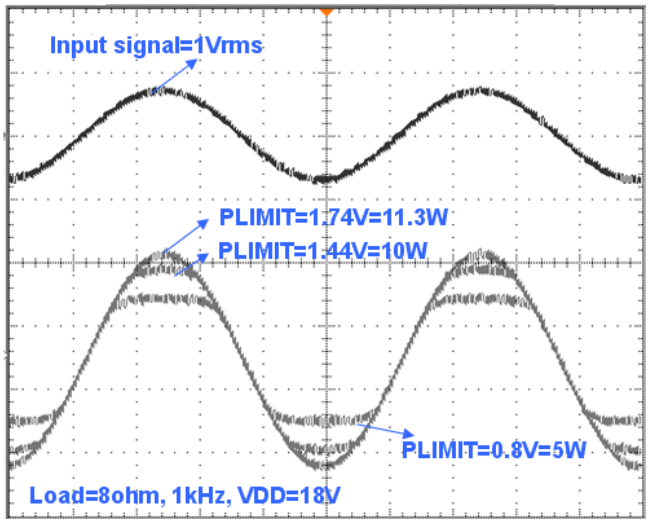

Figure 2. PLIMT Circuit Operation)

The PLIMIT circuit sets a limit on the output peak-to-peak voltage. The limiting is done by limiting the duty cycle to fixed maximum value. This limit can be thought of as a "virtual" voltage rail which is lower than the supply connected to PVCC. This "virtual" rail is 8 times the voltage at the PLIMIT pin. This output voltage can be used to calculate the maximum output power for a given maximum input voltage and speaker impedance.

$$P_{OUT} = \frac{\left(\left(\frac{R_L}{R_L + 2 \times R_S}\right) \times V_P\right)^2}{2 \times R_L}$$

for unclipped power
Where:
R_S is the total output series resistance (including Rdson and the resistance of output filter.
R_L is the load resistance.
V_P is the peak amplifier of the output voltage.
V_P = 8 x PLIMIT voltage if 8 x PLIMIT < PVCC
And

$$P_{OUT}\ @10\%THD \approx 1.25 \times \text{unclipped } P_{OUT}$$

Table 1: Power Limit Typical Operation

Test Condition	PLIMIT Voltage	Output Voltage (Vp-p)	Output Power (~10% THD)
VDD=12V, Vin=1Vrms, Load=8Ω, Gain=20dB	0.80V	14.9	5.0W
VDD=18V, Vin=1Vrms, Load=8Ω, Gain=20dB	0.80V	14.9	5.0W
VDD=18V, Vin=1Vrms, Load=8Ω, Gain=20dB	1.44V	23.6	10.0W
VDD=24V, Vin=1Vrms, Load=8Ω, Gain=20dB	1.44V	23.6	10.0W

Gain Setting

The gain of the MP7751 is set by the input terminals, GAIN0 and GAIN1. The actual gain settings are controlled by ratios of the internal input and feedback resistors, details please see the below table.

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Table 2: Gain Setting

GAIN0	GAIN1	Typ. GAIN (dB)	Typ. Input Impedance (kΩ)
0	0	20	75
1	0	26	50
0	1	32	30
1	1	36	20

Over-Temperature Shutdown

Thermal monitoring is also integrated into the MP7751. If the die temperature rises above 150°C, all switches turn off. The temperature must fall below 130°C before normal operation resumes, with the same power-up sequence used to prevent popping noise.

Short Circuit Performance

The MP7751 has internal overload and short circuit protection. The currents in both the high-side and low-side MOSFETs are measured. Upon detection of short circuit, all MOSFETs of the over current full bridge channel will go into high impedance for a fixed duration before resuming normal operation. After the fixed duration and the short circuit condition is removed, the MP7751 will restart with the start up sequence that is used for normal starting to prevent a pop from occurring.

Fault Output

The MP7751 includes an open drain, active low fault indicator output on the /FAULT pin. A fault triggers if either the current limit or thermal shutdown is tripped.

A fault on any channel will cause the FAULTB pin to pull low. A fault on either channel will cause the all outputs to go into high impedance. When the fault goes away, the MP7751 will resume normal operation.

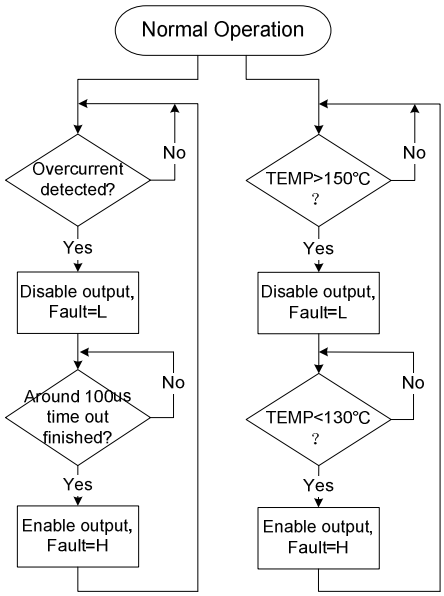

Figure 3: Fault Timing Chart

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APPLICATION INFORMATION

COMPONENT SELECTION

Delay time for input signal absence report

The Recovery time is defined as follows.

$$T_{delay} = 1.6 \times 10^8 \times C_R [sec]$$

Choosing the Output LC Filter

The inductor-capacitor (LC) filter converts the pulses at SW to the output voltage that drives the speaker. There are two kinds of LC filter structure depending on the output configuration.

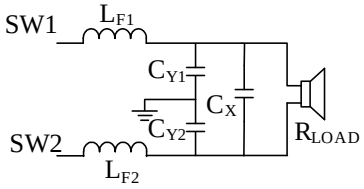

Figure 4: BTL Filter Configuration

Where:

$$L_F = L_{F1} + L_{F2},$$

$$C_F = C_X + \frac{C_{Y1} \times C_{Y2}}{C_{Y1} + C_{Y2}},$$

$$L_{F1} = L_{F2};$$

$$C_{Y1} = C_{Y2}$$

The characteristic frequency of the LC filter needs to be high enough to allow high frequency audio to the output, yet needs to be low enough to filter out high frequency products of the pulses from the SW pin. The characteristic frequency of the LC filter is:

$$f_0 = \frac{1}{2 \times \pi \times \sqrt{L_F \times C_F}}$$

The quality factor (Q) of the LC filter is important: If this is too low, output noise will increase; if this is too high, then peaking may occur at high frequencies and reduce the passband flatness. The circuit Q is set by the load resistance (speaker resistance, typically 4Ω or 8Ω). Q is calculated as:

$$Q = \frac{R_{LOAD}}{\omega_0 \times L_F} = \frac{R_{LOAD}}{2\pi \times f_0 \times L_F}$$

ω_0 is the characteristic frequency in radians/second and f_0 is in Hz. Use an LC filter with Q between 0.7 and 1.4.

The type of inductor and capacitor used in the LC filter greatly affects the output ripple and noise. Use a film capacitor and an inductor with sufficient power rating to supply the output current to the load. The inductor must exhibit soft saturation characteristics: If the inductor exhibits hard saturation, it should operate well below the saturation current. Use toroidal cores made of gapped ferrite, MPP, powdered iron, or similar materials. If using either an open or shielded bobbin ferrite core for multi-channel designs, make sure that the start windings of each inductor align (all starting toward the SW pin, or all starting toward the output) to prevent crosstalk or other channel-to-channel interference.

Input Coupling Capacitor

The input coupling capacitor transmits the AC signal from the source to the MP7751 while blocking the DC voltage. Choose an input coupling capacitor such that the corner frequency (f_{IN}) is less than the passband frequency. The corner frequency is calculated as:

$$f_{IN} = \frac{1}{2 \times \pi \times R_{IN} \times C_{IN}}$$

The impedance of the input resister is different with the different gain setting. At the same gain setting, the input impedance from part-to-part may shift by ±20% due to shifts in the actual resistance of the input resistors. But please note that the gain variation from part-to-part is small.

For design purposes, the input network should be designed assuming an input impedance of 16 kΩ, which is the absolute minimum input impedance of the MP7751. At the lower gain settings, the input impedance could increase as high as 90 kΩ.

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Power Source

For maximum output power, the amplifier circuit requires a regulated external power source. A high power-supply voltage can deliver more power to a given load resistance, but a power-source voltage exceeding the maximum voltage of 26V can damage the MP7751. The MP7751's power supply rejection is excellent, though power-supply noise can pass to the output, so care must be taken to minimize power supply noise within the pass-band frequencies. Bypass the power supply with a large capacitor (typically aluminum electrolytic) along with two smaller 1μF and 1nF ceramic capacitors at the MP7751 VCC supply pins.

PCB Layout

Circuit layout is critical for optimal performance, low output distortion, and noise. Duplicate the EVB layout for best results. For layout changes, follow these guidelines and use Figure 7 and Figure 8 as references.

1) Place the following components as close to the MP7751 as possible:

Bootstrap Capacitors

C_{BS} supply the gate drive current to the internal HS-FET. Place C_{BS} as close to BST pin and SW pin as possible.

Power Supply Bypass Capacitors

C_{BYP} carry the transient current for the switching power stage. To avoid overstressing the MP7751 and excessive output noise, place C_{BYP} as close to the PVCC pins as possible.

2) The Inductor-Capacitor (LC) filter converts the pulse train at SW to the output voltage that drives the speaker. Please keep the filter capacitor close to the inductor.

3) Make sure that any traces carrying the switch node (SW) voltages are routed far from any input signal traces. If the trace must run near the SW trace near the input, shield the input with a ground plane between the traces. Physically separate each channel to prevent crosstalk. Make sure that all inductors used on a single circuit board have the same orientation.

Route each power supply from the source to each channel individually, not serially. This prevents channel-to-channel coupling through the power supply input.

Electro-Magnetic Interference (EMI) Considerations

Due to the switching nature of Class D amplifiers, care must be taken to minimize the effects of electromagnetic interference from the amplifier. However, proper component selection and careful attention to circuit layout can minimize the effects of the EMI due to the amplifier switching.

The power inductors are a potential source of radiated emissions. For the best EMI performance, use toroidal inductors, since the magnetic field is well-contained inside the core. However toroidal inductors can be expensive to wind. For a more economical solution, use shielded-gapped–ferrite or shielded-ferrite-bobbin-core inductors. These inductors typically do not contain the EM field as well toroidal inductors, but can achieve a better balance between good EMI performance with low cost.

The size of high-current loops that carry rapidly changing currents must be minimized: Make sure that the V_{CC} bypass capacitors are as close to the MP7751 as possible.

Nodes that carry rapidly changing voltage, such as SW, need to be made as small as possible. If sensitive traces run near a trace connected to SW, place a ground shield between the traces.

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TYPICAL APPLICATION CIRCUITS

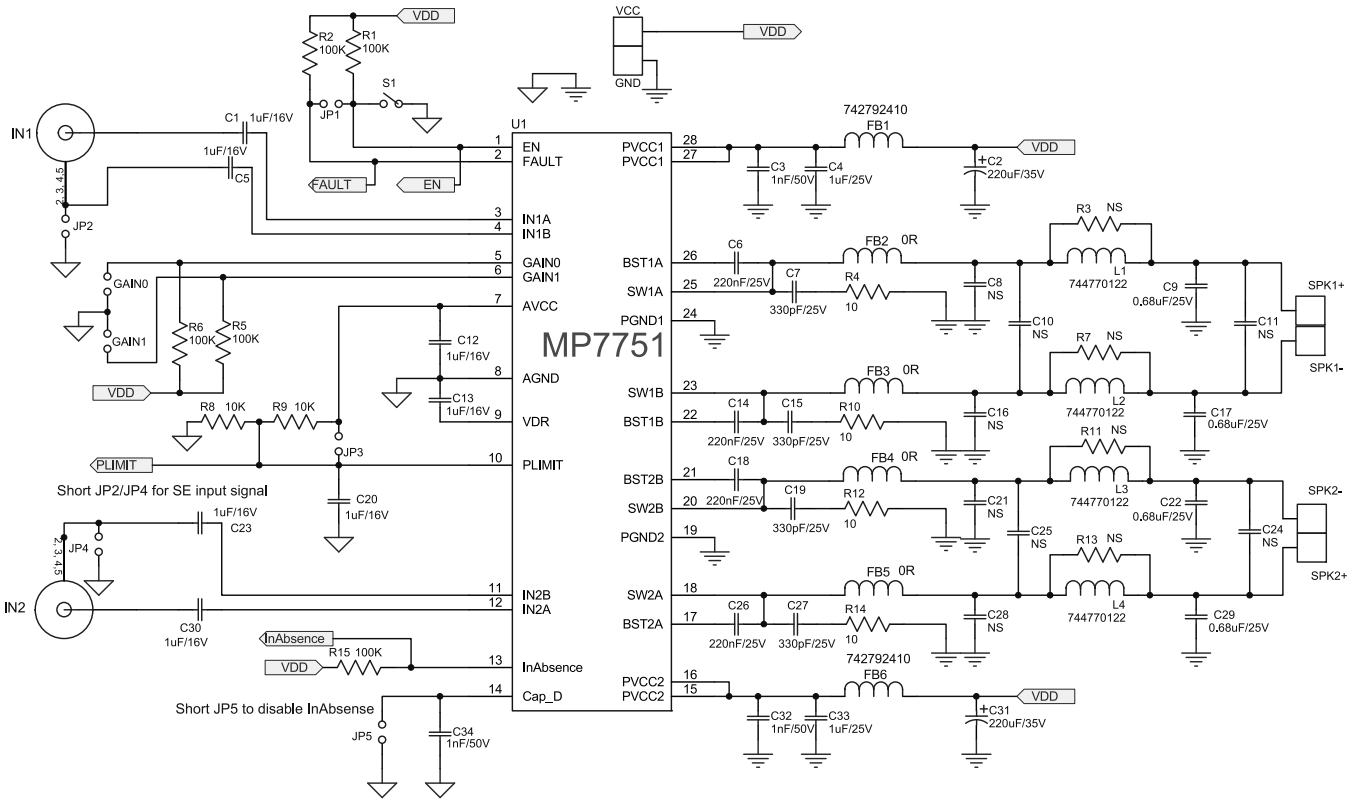

Figure 5: Typical Application Circuit

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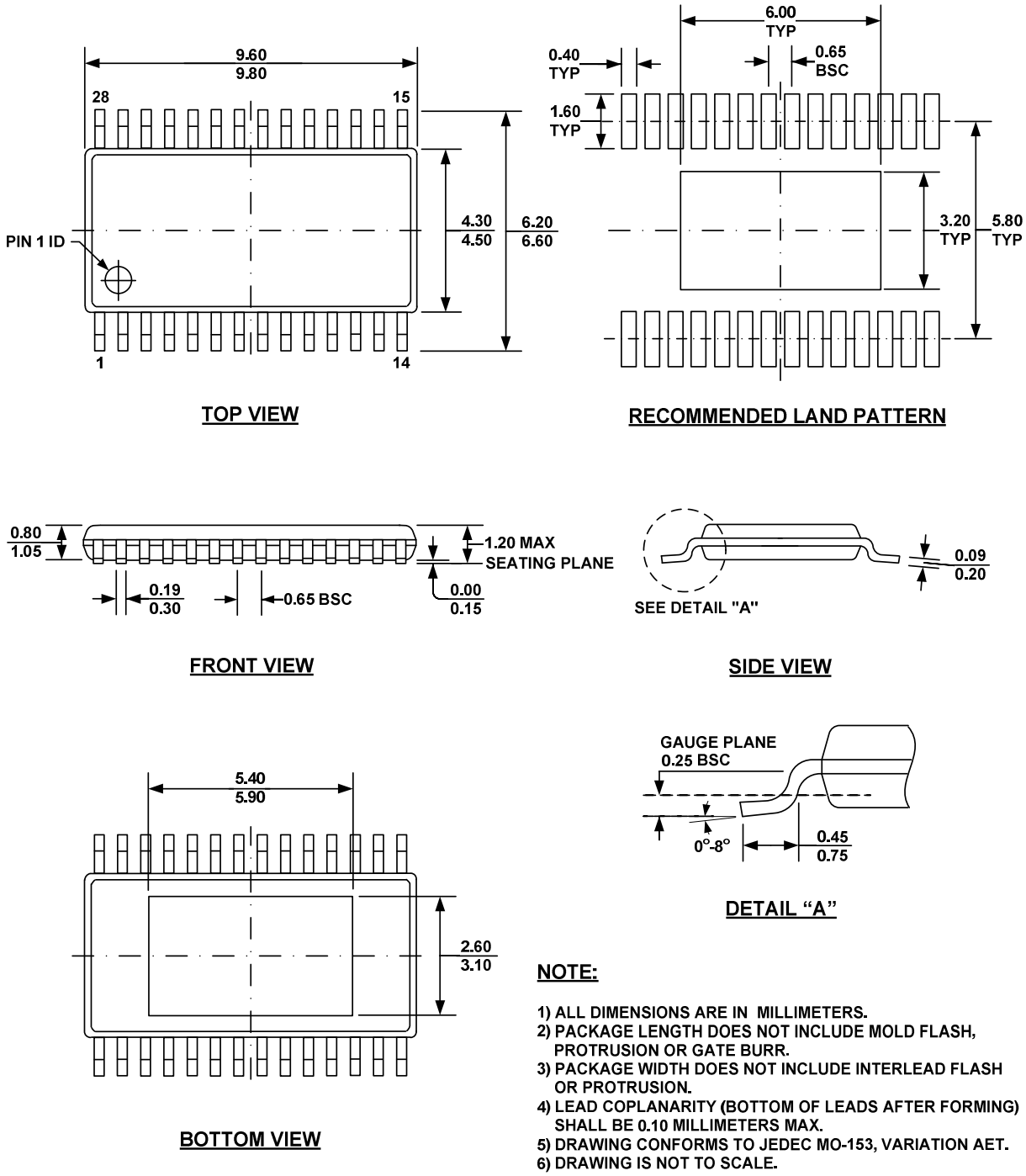
PACKAGE INFORMATION

TSSOP-28 EP



NOTE:

1) ALL DIMENSIONS ARE IN MILLIMETERS.
2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH, PROTRUSION OR GATE BURR.
3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION.
4) LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.10 MILLIMETERS MAX.
5) DRAWING CONFORMS TO JEDEC MO-153, VARIATION AET.
6) DRAWING IS NOT TO SCALE.

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