



MP6519A

2.5V to 28V, 5A, Full H-Bridge Current Regulator

DESCRIPTION

The MP6519A is a monolithic, step-down, current-source driver for applications that require accurate and fast current response control. The MP6519A achieves up to 5A of output current (I_{OUT}), with excellent load and line regulation across a wide input voltage (V_{IN}) supply range.

The MP6519A provides H-bridge control with four integrated MOSFETs to achieve fast dynamic load response and an ultra-high efficiency solution. For ease of use, the output polarity can be controlled by pulling the MODE pin high or low.

By setting the full-scale I_{OUT} through an external resistor, I_{OUT} can be dimmed by the pulse-width modulation (PWM) input signal from 0% to 100% of the full-scale current range.

Full protection features include open-load protection, load-short protection, over-current protection (OCP), over-temperature protection (OTP), and input over-voltage protection (OVP).

The MP6519A is available in a QFN-19 (3mmx3mm) package.

FEATURES

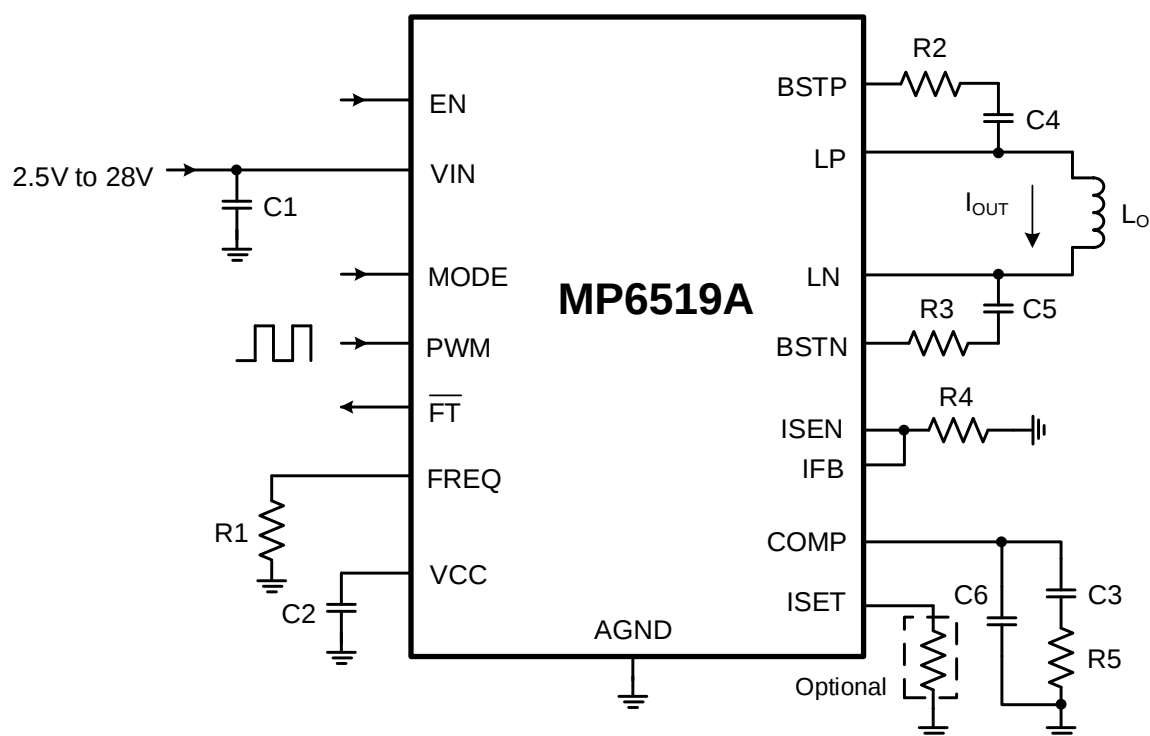
- Wide 2.5V to 28V Operating Input Voltage (V_{IN}) Range
- Up to 5A of Output Current (I_{OUT})
- $\pm 2\%$ Accuracy at Full-Scale Output Current (I_{OUT_FULL}) Reference
- 65m Ω On Resistance ($R_{DS(ON)}$) for Each MOSFET of the H-Bridge
- 100% Duty Cycle Operation of the H-Bridge
- 30kHz to 300kHz Configurable Switching Frequency (f_{SW})
- 20kHz to 100kHz Pulse-Width Modulation (PWM) Input for Current Regulation
- Configurable I_{OUT_FULL}
- Up to 94% Efficiency
- Selectable Current Polarity Mode
- Switching Automatically Disabled by PWM Input Detection
- 1 μ A Shutdown Mode
- Inherent Open-Load Protection
- Cycle-by-Cycle Over-Current Protection (OCP)
- Output Short-Circuit Protection (SCP)
- Input Over-Voltage Protection (OVP)
- Over-Temperature (OT) Shutdown
- Available in a QFN-19 (3mmx3mm) Package

APPLICATIONS

- Current Regulators
- DC Motors
- Solenoids and Actuators

All MPS parts are lead-free, halogen-free, and adhere to the RoHS directive. For MPS green status, please visit the MPS website under Quality Assurance. "MPS", the MPS logo, and "Simple, Easy Solutions" are trademarks of Monolithic Power Systems, Inc. or its subsidiaries

TYPICAL APPLICATION



ORDERING INFORMATION

Part Number*	Package	Top Marking	MSL Rating
MP6519AGQ	QFN-19 (3mmx3mm)	See Below	1

* For Tape & Reel, add suffix -Z (e.g. MP6519AGQ-Z).

TOP MARKING

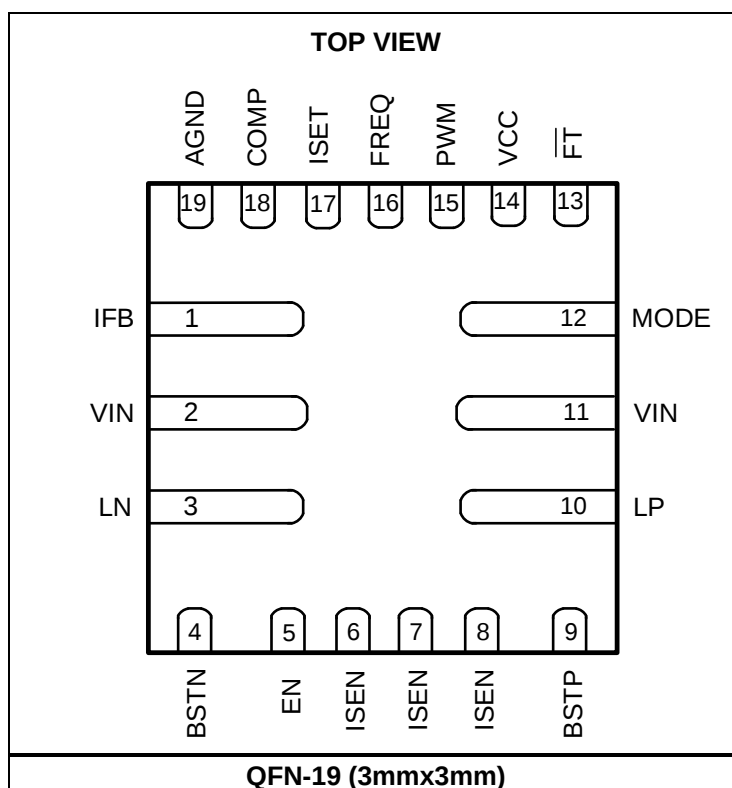
CCQY
LLLL

CCQ: Product code

Y: Year code

LLLL: Lot number

PACKAGE REFERENCE



PIN FUNCTIONS

Pin #	Name	Description
1	IFB	Current-sense signal feedback. Connect the IFB and ISEN pins together.
2, 11	VIN	Input supply.
3	LN	Negative switching node of the H-bridge.
4	BSTN	Bootstrap for the LN high-side MOSFET (HS-FET) gate driver. Connect a capacitor between the BSTN and LN pins.
5	EN	IC enable.
6, 7, 8	ISEN	Current sense. Connect a current-sense resistor between the ISEN pin and power ground.
9	BSTP	Bootstrap for the LP HS-FET gate driver. Connect a capacitor between the BSTP and LP pins.
10	LP	Positive switching node of the H-bridge.
12	MODE	Current polarity setting. If the current direction flowing from LP to LN is positive, pull the MODE pin high to run the current from LP to LN; pull MODE low to run the current from LN to LP.
13	$\overline{\text{FT}}$	Fault indication output. The $\overline{\text{FT}}$ pin is active low for fault conditions.
14	VCC	5V low-dropout (LDO) output for internal driver and logic.
15	PWM	Pulse-width modulation (PWM) signal input for current dimming. Apply a >20kHz PWM signal to the PWM pin.
16	FREQ	Switching frequency setting. Connect a resistor between the FREQ pin and AGND.
17	ISET	Full-scale current reference setting. Connect a resistor between AGND and the ISET pin.
18	COMP	Loop compensation setting.
19	AGND	Ground for internal logic.

ABSOLUTE MAXIMUM RATINGS ⁽¹⁾

Supply voltage (V_{IN}) 35V
 $V_{\text{LP}}, V_{\text{LN}}$ -0.3V to $V_{\text{IN}} + 0.3\text{V}$
 V_{BSTP} $V_{\text{LP}} + 6\text{V}$
 V_{BSTN} $V_{\text{LN}} + 6\text{V}$
All other pins -0.3V to +6V
Continuous power dissipation ($T_{\text{A}} = 25^{\circ}\text{C}$) ⁽²⁾
QFN-19 (3mmx3mm) 2.5W
Junction temperature (T_{J}) 150°C
Lead temperature 260°C
Storage temperature -65°C to +150°C

ESD Ratings

Human body model (HBM) ±2kV
Charged-device model (CDM) ±750V

Recommended Operating Conditions ⁽³⁾

Supply voltage (V_{IN}) 2.5V to 28V
Operating junction temp (T_{J}) -40°C to +125°C

Thermal Resistance ⁽⁴⁾ θ_{JA} θ_{JC}
QFN-19 (3mmx3mm) 50 8 °C/W

Notes:

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature, T_{J} (MAX), the junction-to-ambient thermal resistance, θ_{JA} , and the ambient temperature, T_{A} . The maximum allowable continuous power dissipation at any ambient temperature is calculated by P_{D} (MAX) = $(T_{\text{J}}$ (MAX) - T_{A}) / θ_{JA} . Exceeding the maximum allowable power dissipation produces an excessive die temperature, which may cause the regulator to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 3) The device is not guaranteed to function outside of its operation conditions.
- 4) Measured on a JESD51-7, 4-layer board.

ELECTRICAL CHARACTERISTICS

$V_{IN} = 12V$, $T_A = 25^{\circ}C$, unless otherwise noted.

Parameters	Symbol	Condition	Min	Typ	Max	Units
Supply Voltage						
VIN operating range	VIN		2.5		28	V
Turn-on threshold	VIN_ON	VIN rising edge		2.3	2.45	V
Turn-on hysteric voltage	VIN_HY			0.15		V
IC Supply						
Shutdown current	IIN_SD	EN = low			1	μA
Quiescent current	IIN_SBY	Standby mode		370	450	μA
VCC regulator voltage	VCC	VIN > 5.2V	4.5	5	5.5	V
VCC regulator dropout voltage		VIN < 5V, 20mA load		100		mV
Logic						
Enable (EN) high threshold	VEN_HIGH				1.5	V
EN low threshold	VEN_LOW		0.4			V
MODE input high threshold	VEN_HIGH				1.5	V
MODE input low threshold	VEN_LOW		0.4			V
Pulse-width modulation (PWM) high threshold	VPWM_HIGH				1.5	V
PWM low threshold	VPWM_LOW		0.4			V
IC start-up delay	tDELAY	EN active to switching		230	350	μs
Switching Frequency						
Switching frequency	fsw	RREQ = 75kΩ	255	300	345	kHz
		RREQ = 750kΩ	22	30	38	kHz
Current Reference						
Current reference accuracy	VREF_FB	VREF_FB = 200mV	196	200	204	mV
		VREF_FB = 100mV	97	99	101	mV
Loop Compensation						
Transconductance	GEA			270		μA/V
Maximum source current				50		μA
Maximum sink current				50		μA
Power MOSFET						
High-side MOSFET (HS-FET) on resistance	RDS(ON)_HS		42	65	93	mΩ
Low-side MOSFET (LS-FET) on resistance	RDS(ON)_LS		42	65	93	mΩ
Minimum on time				200		ns
Bootstrap for High-Side (HS) Driver						
Forward voltage for bootstrap charge				0.5		V
Bootstrap under-voltage lockout (UVLO) threshold		Rising edge		2		V

ELECTRICAL CHARACTERISTICS *(continued)*

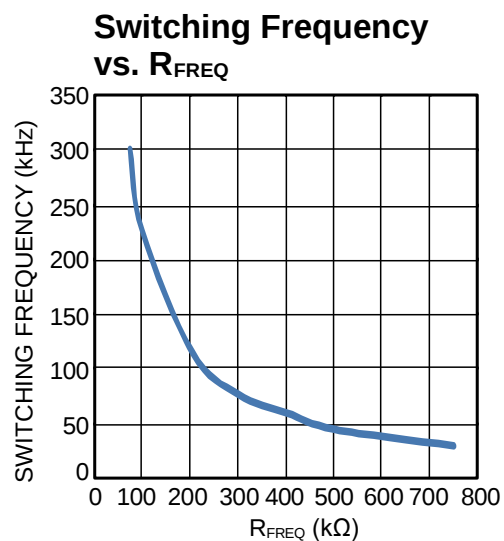
$V_{IN} = 12V$, $T_A = 25^{\circ}C$, unless otherwise noted.

Parameters	Symbol	Condition	Min	Typ	Max	Units
Protection						
Hiccup over-current (OC) threshold		Float R_{ISET}	255	300	345	mV
Load short hiccup recovery time				1		ms
Latch-off OC threshold		Float R_{ISET} , $R_{SEN} = 40m\Omega$		13		A
Input over-voltage protection (OVP) threshold	V_{IN_OVP}		28.2	30	31	V
Thermal shutdown ⁽⁵⁾				150		$^{\circ}C$
Thermal shutdown hysteresis				20		$^{\circ}C$

Note:

5) Guaranteed by design.

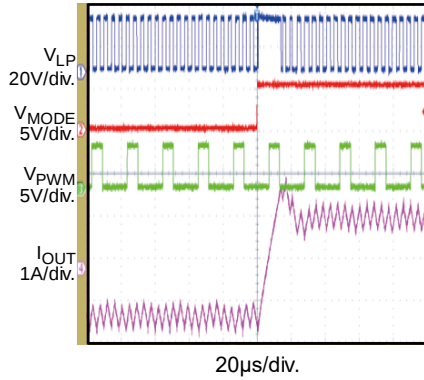
TYPICAL CHARACTERISTICS



TYPICAL PERFORMANCE CHARACTERISTICS

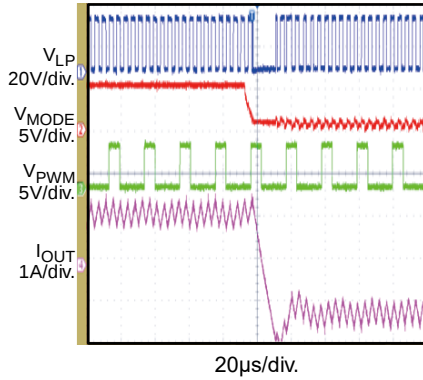
Mode Transfer

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE low to high, $1\Omega + 100\mu H$ load



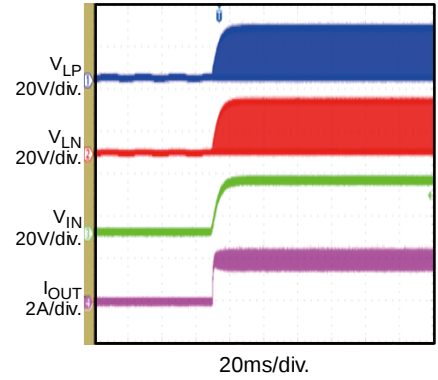
Mode Transfer

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE high to low, $1\Omega + 100\mu H$ load



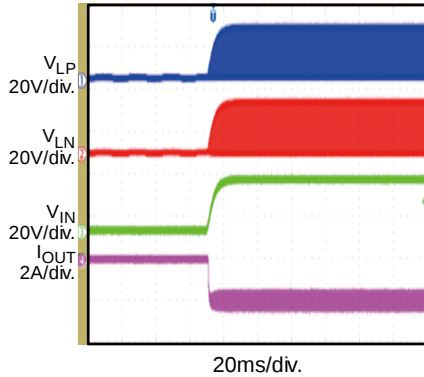
Start-Up through VIN

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = high $1\Omega + 100\mu H$ load



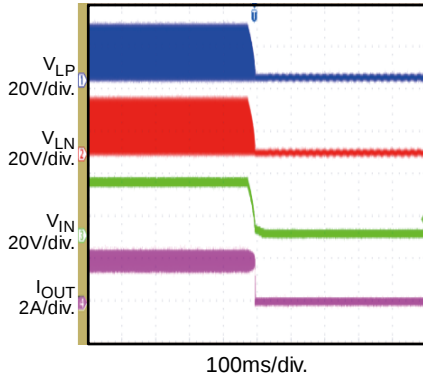
Start-Up through VIN

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = low, $1\Omega + 100\mu H$ load



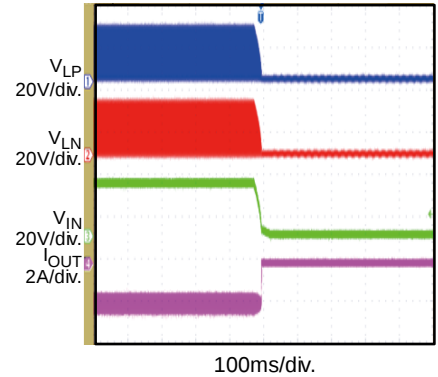
Shutdown through VIN

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = high, $1\Omega + 100\mu H$ load



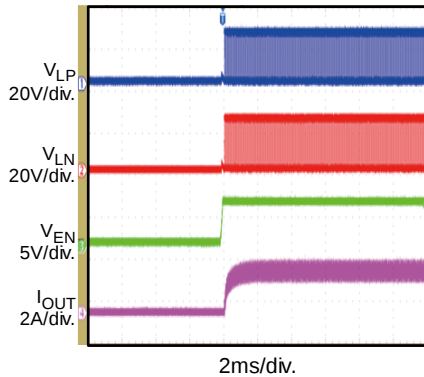
Shutdown through VIN

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = low, $1\Omega + 100\mu H$ load



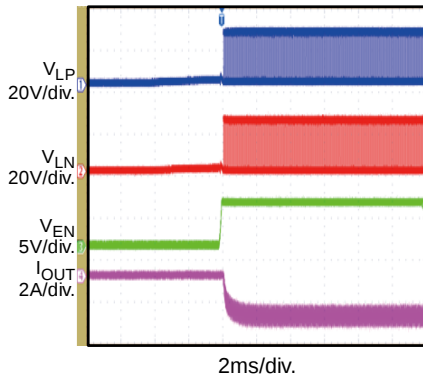
Start-Up through EN

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = high, $1\Omega + 100\mu H$ load



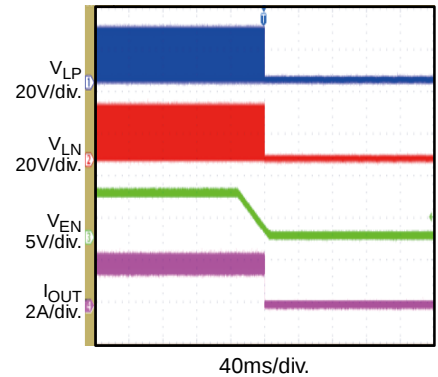
Start-Up through EN

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = low, $1\Omega + 100\mu H$ load



Shutdown through EN

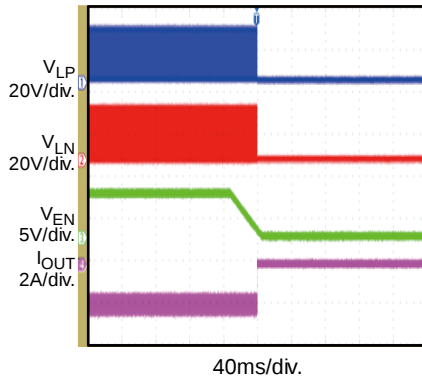
$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = high, $1\Omega + 100\mu H$ load



TYPICAL PERFORMANCE CHARACTERISTICS (continued)

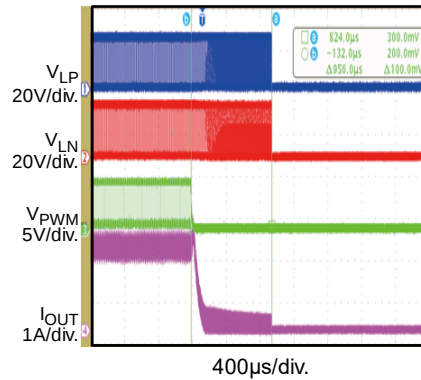
Shutdown through EN

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = low, $1\Omega + 100\mu H$ load



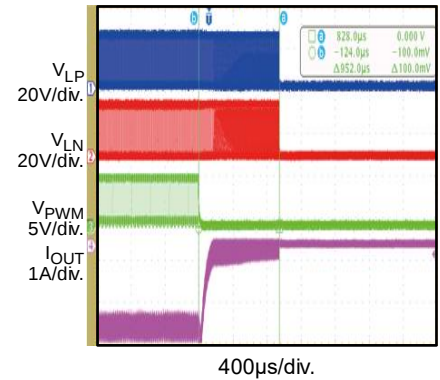
Sleep Entry

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = high, $1\Omega + 100\mu H$ load



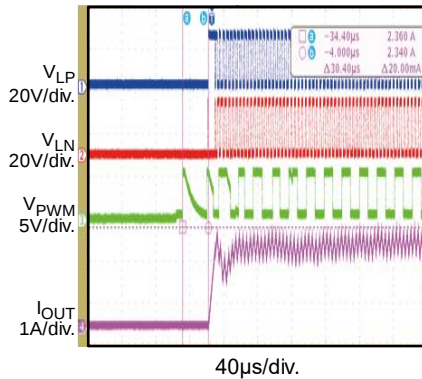
Sleep Entry

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = low, $1\Omega + 100\mu H$ load



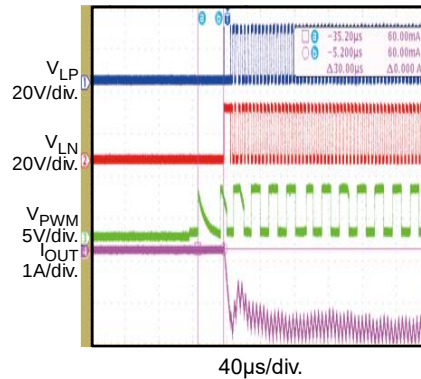
Sleep Recovery

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = high, $1\Omega + 100\mu H$ load



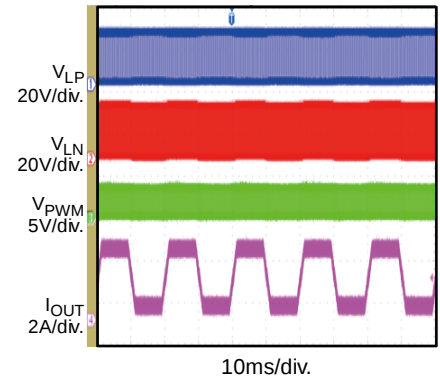
Sleep Recovery

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = low, $1\Omega + 100\mu H$ load



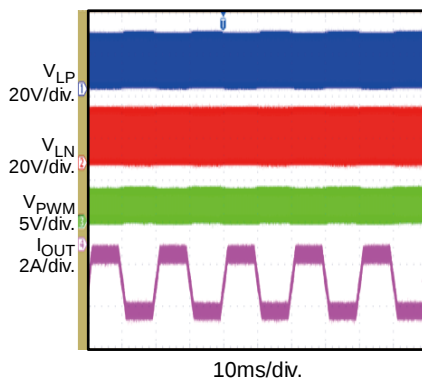
Trapezoidal Wave

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = high, $1\Omega + 100\mu H$ load



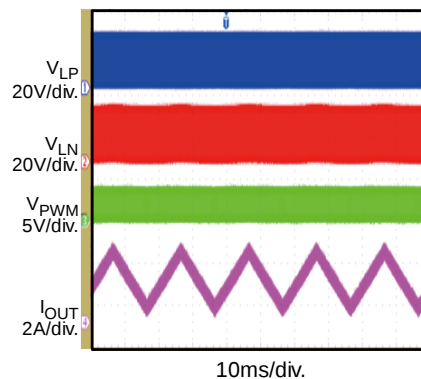
Trapezoidal Wave

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = low, $1\Omega + 100\mu H$ load



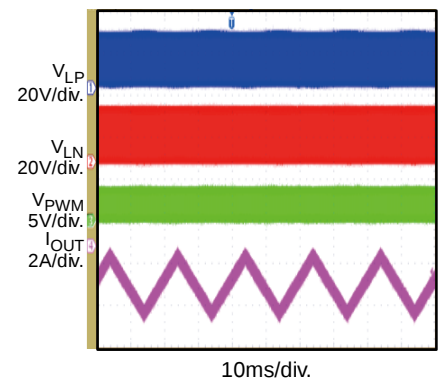
Triangle Wave

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = high, $1\Omega + 100\mu H$ load



Triangle Wave

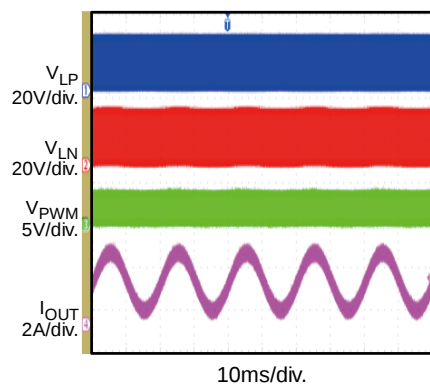
$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = low, $1\Omega + 100\mu H$ load



TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

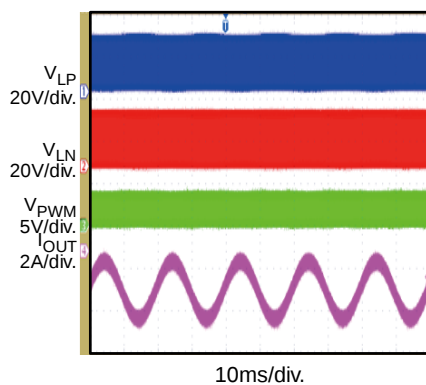
Sine Wave

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = high, $1\Omega + 100\mu H$ load



Sine Wave

$V_{IN} = 24V$, $V_{EN} = 5V$, duty = 50%,
MODE = low, $1\Omega + 100\mu H$ load



FUNCTIONAL BLOCK DIAGRAM

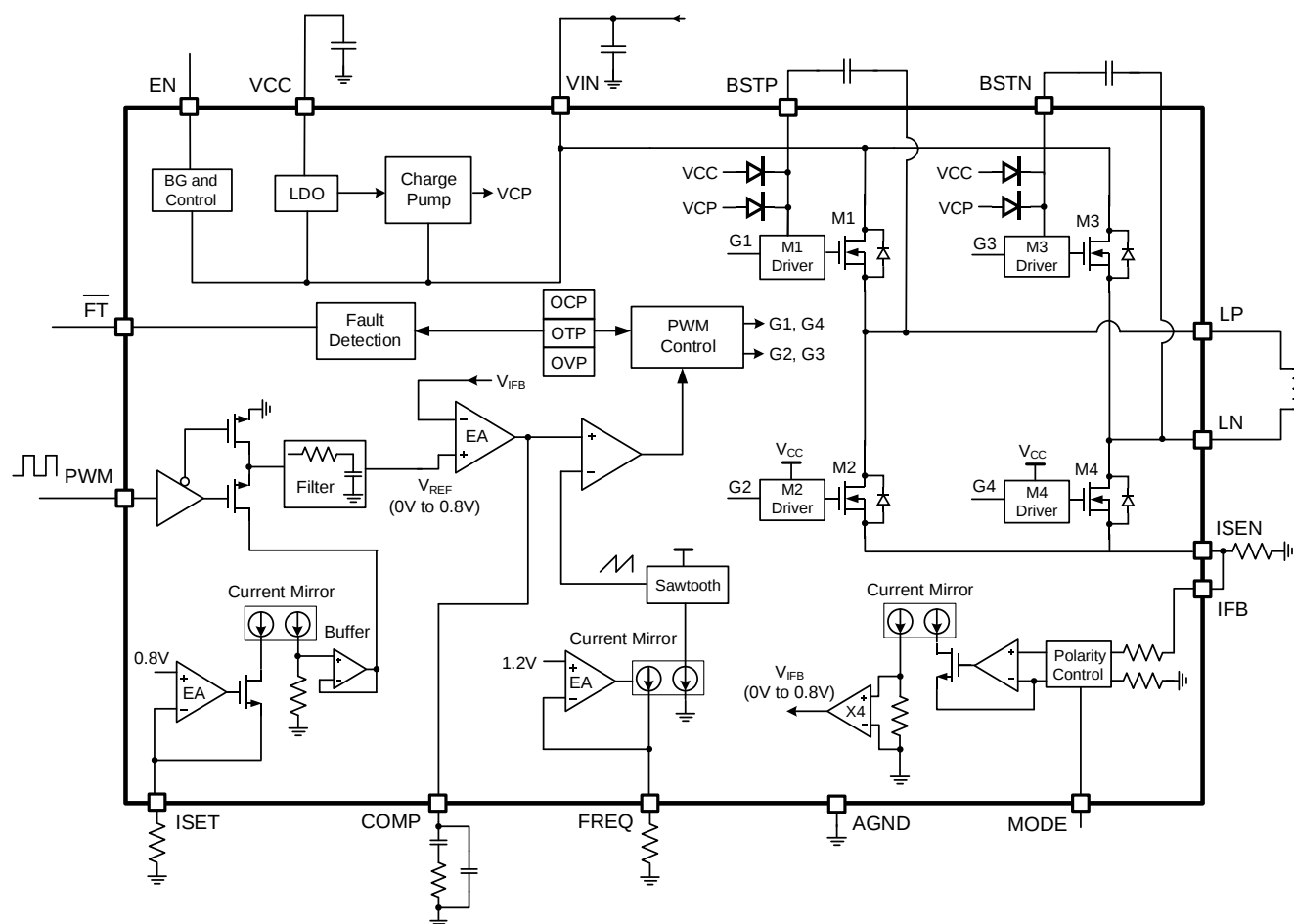


Figure 1: Functional Block Diagram

OPERATION

The MP6519A is a current driver for applications that require accurate load current (I_{LOAD}) control and fast dynamic current response. The MP6519A works in step-down mode with four fully integrated MOSFET H-bridges (M1, M2, M3, and M4) to provide small size and high efficiency. The full-scale output current (I_{OUT_FULL}) can be set by the external resistor, and the current polarity can be controlled by the MODE pin to set the bidirectional current.

H-Bridge General Operation

The MP6519A works in a quad-MOSFET H-bridge topology and uses pulse-width-modulation (PWM) with average current control to achieve a bidirectional current output and fast dynamic current response. The switching frequency (f_{SW}) is configurable between 30kHz and 300kHz.

When enabled in normal operation, M1 and M4, turn on and off in the same sequence, and M2 and M3 turn on and off in the same sequence. M1/M4 and M2/M3 turn on and off in complementary operation with a dead time (DT) of about 25ns to avoid damage to the device due to shoot-through. All the MOSFET switches have a minimum on time of about 200ns. If the I_{OUT} direction is set to positive by pulling the MODE pin high, then I_{OUT} sensed by M2 and M4 is sent to the negative input of the error amplifier (EA). By comparing the I_{OUT} feedback signal with the current reference signal at the EA's positive node, the EA outputs an appropriate voltage that is compared with a sawtooth signal to provide a driver signal for M1/M4 and M2/M3. The device can enter four different modes to control the working sequence: shutdown mode, standby mode, normal switching mode, and current polarity mode.

Shutdown Mode

When the enable (EN) signal is pulled low, the MP6519A enters shutdown mode. In this mode, all circuits and blocks are disabled, and the MP6519A consumes below 1 μ A of shutdown current (I_{IN_SD}). There is a deglitch time of about 150ns to avoid mistriggering EN shutdown.

Standby Mode

The MP6519A enters standby mode if either of the following conditions is met:

- During start-up, the PWM signal on the PWM pin is low while EN is high.
- After start-up in normal switching operation, the PWM signal remains low for longer than 1ms if EN is high.

In this mode, the bandgap block and other control blocks begin working, except for the gate drive block of the internal switching MOSFETs. The device stops switching to reduce the quiescent current (I_{IIN_SBY}) at no load. Standby mode can also minimize the time during which I_{OUT} tracks the reference signal of the PWM input, which occurs after the EN signal. Since the MP6519A requires some time to establish the bandgap signal and other required control blocks, it is recommended to apply the PWM signal after a minimum of 300 μ s passes from the EN signal switching high.

Normal Switching Mode

If both the PWM and EN signals remain high, then the MP6519A enters normal switching mode immediately. In this mode, the feedback I_{OUT} closely follows the reference signal, which is received from the PWM input signal through an RC filter (for more details, see the Current Feedback section on page 14 and the Pulse-Width Modulation (PWM) Input Current Dimming section on page 13).

The H-bridge MOSFETs work with a fixed f_{SW} (see the Setting the Switching Frequency section on page 13). The I_{OUT} polarity can be changed easily by pulling MODE high or low (see the Current Polarity Mode section below).

Current Polarity Mode

The current polarity is set by MODE. If MODE is pulled high, the current is positive, and the current direction goes from LP to LN. By pulling MODE low, the current is negative, and the current direction goes from LN to LP. There is a deglitch time of about 150ns to avoid mistriggering changes in current polarity mode.

Setting the Full-Scale Output Current

The full-scale I_{OUT} reference voltage (V_{REF_FULL}) is set by connecting a resistor between the ISET pin and AGND. When ISET is floated, V_{REF_FULL} is set to 200mV by default. If a resistor is connected between ISET and AGND, then V_{REF_FULL} can be reduced below 200mV to reduce power loss on the feedback resistor. The MP6519A requires about 0.3ms to detect whether a resistor is available on ISET when the IC starts up for the first time. During this time, the MP6519A is not switching. V_{REF_FULL} can be calculated with Equation (1):

$$V_{REF_FULL} = 0.2 \times \frac{40}{R_{ISET} (k\Omega)} \quad (1)$$

For example, if the ISET resistance (R_{ISET}) is 80k Ω , then the reference voltage is 100mV. For improved accuracy, a 40k Ω to 80k Ω R_{ISET} is recommended to achieve a 200mV to 100mV current reference voltage.

Start-Up Sequence

The MP6519A requires about 0.3ms to detect whether a resistor is available on ISET when the IC starts up for the first time. During this time, the MP6519A is not switching. It is recommended to apply a PWM signal after a minimum of 0.3ms passes from the EN signal (see Figure 2 and Figure 3).

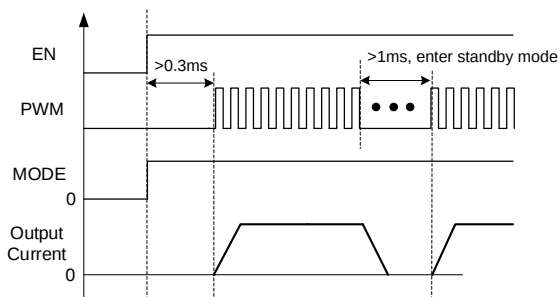


Figure 2: Positive Output Current Mode

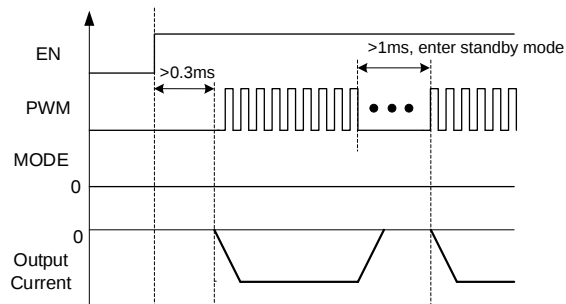


Figure 3: Negative Output Current Mode

Setting the Switching Frequency

The H-bridge MOSFET's f_{SW} is set by connecting a resistor between the FREQ pin and AGND. With a proper resistance, f_{SW} can be set between 30kHz and 300kHz. A higher f_{SW} results in smaller current ripple; however, the MOSFETs' switching loss is also larger. Therefore, a tradeoff is required for the design. The FREQ frequency (f_{FREQ}) can be calculated with Equation (2):

$$f_{FREQ} = \frac{22500}{R_{FREQ} (k\Omega)} \quad (2)$$

Pulse-Width Modulation (PWM) Input Current Dimming

If V_{REF_FULL} is set, then the actual I_{OUT} reference voltage (V_{REF_FB}) sent to the EA can be further controlled by applying a PWM input signal to the PWM pin. As a result, V_{REF_FULL} is chopped by the PWM input signal, and the current reference voltage is received from this chopped PWM voltage through the internal low-pass filter. For a smaller I_{OUT} reference ripple, the PWM input frequency is recommended to be between 20kHz and 100kHz. Considering the full-scale reference, V_{REF_FB} can be calculated with Equation (3):

$$V_{REF_FB} = 0.2 \times \frac{40}{R_{ISET} (k\Omega)} \times D_{PWM} \quad (3)$$

Where D_{PWM} is the duty cycle of the PWM input.

Current Feedback

The current flowing through the load is sensed via a resistor connected between the IFB pin and AGND. This sensing voltage on IFB is sent to the feedback block circuit and used to generate the average feedback voltage (V_{IFB}),

which is equal to the average I_{OUT} multiplied by the sensing resistance (R_{IFB}). V_{IFB} is sent to the EA's negative node and compared with the I_{OUT} reference voltage on the EA's positive node. The EA output is COMP, and the COMP voltage (V_{COMP}) generates the internal MOSFET switch's on and off times. Figure 4 shows the current feedback loop.

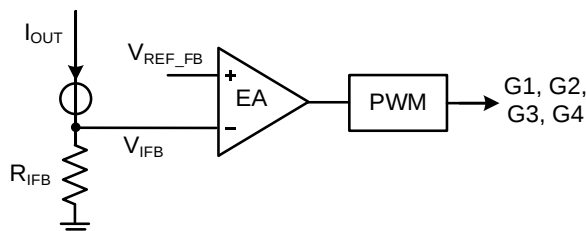


Figure 4: Current Feedback Loop

VCC Low-Dropout (LDO) Regulator

The MP6519A employs a low-dropout (LDO) regulator to provide a constant voltage (5V) at VCC. The VCC voltage (V_{CC}) is used for the internal power supply of the logic circuit and driver circuit. When the input voltage (V_{IN}) is sufficiently high (exceeds 5.2V), the VCC output is 5V. When V_{IN} drops below 5V, V_{CC} drops with V_{IN} . The dropout voltage is about 100mV. If V_{CC} drops below 2.15V, then the IC triggers a power reset sequence and shuts down. The IC resumes normal operation when V_{CC} exceeds 2.3V.

High-Side MOSFET (HS-FET) Driver

M1 and M3's high-side MOSFETs (HS-FETs) are N-channel MOSFETs. When M1 and M3 turn on, a bootstrap supply voltage across the BSTP and BSTN pins is required. The bootstrap voltage (V_{BST}) is generated by a combination of the internal charge pump and a 5V VCC. This allows the IC to work at 100% duty cycle to provide sufficient driver voltage for M1 and M3's HS-FETs.

Over-Current Protection (OCP)

To provide robust protection during an over-current (OC) event, the IC uses a two-level protection mode.

If the current flowing through the MOSFETs exceeds 150% of the full-scale setting value during two consecutive switching cycles, then the IC stops switching and triggers a power reset sequence to restart after 1ms.

If the current flowing through the MOSFETs exceeds 200% of the full-scale setting value, then the IC latches off. If the HS-FET triggers an OC fault, the HS-FET turns off immediately and the $\overline{FT}$ pin is pulled low. At the same time, the two low-side MOSFETs (LS-FETs) turn on for several ms before turning off, and the IC latches off. If the LS-FET triggers an OC fault, the LS-FET turns off immediately and the $\overline{FT}$ pin is pulled low. At the same time, the HS-FETs turn on for several ms before turning off, and the IC latches off.

Input Over-Voltage Protection (OVP)

During operation, the energy stored in I_{LOAD} is delivered to the input side during the free-wheeling time. If V_{IN} and I_{OUT} are sufficiently high, the energy sent back to the input side causes V_{IN} to rise. The MP6519A employs V_{IN} protection to avoid damage to the IC due to a high voltage spike. If V_{IN} exceeds the input over-voltage (OV) threshold for four consecutive switching cycles, then the IC stops switching and latches off immediately.

Junction Over-Temperature Protection (OTP)

If the IC's junction temperature (T_J) exceeds 150°C, then the IC stops switching. Once T_J drops below 130°C, the IC resumes normal operation.

Fault Indication Output ($\overline{FT}$)

During normal operation, $\overline{FT}$ is a high-impedance open-drain pin. If any fault occurs during operation, $\overline{FT}$ pulls low to indicate the fault condition for the external system. Recycle the input power or toggle the EN signal to remove the fault latch condition.

Enable (EN)

To enable the IC, a logic-high signal must be applied to EN, and the high-level signal time must be longer than 10μs. To shut down the IC, pull EN to logic low, and the low-level signal must be longer than 100ns.

APPLICATION INFORMATION

Selecting the Input Capacitor

The input capacitor (C_{IN}) reduces the surge current drawn from the input supply as well as the device's switching noise. The impedance of C_{IN} at f_{SW} must be below the input source impedance to prevent the high-frequency switching current from passing through to the input. Ceramic capacitors with X5R or X7R dielectrics are recommended for their low-ESR and small temperature coefficients. A larger-value capacitor is helpful for reducing V_{IN} ripple and noise. For most applications, two 22 μ F ceramic capacitors in parallel are sufficient. It is recommended to connect a capacitor on each VIN pin.

Setting the Full-Scale Output Current

If a resistor is connected between ISET and AGND, I_{OUT} can be calculated with Equation (4):

$$I_{OUT} = 0.2 \times \frac{40}{R_{ISET} (k\Omega)} \times \frac{1}{R_{IFB} (\Omega)} \quad (4)$$

If ISET is floated, I_{OUT} can be calculated with Equation (5):

$$I_{OUT} = \frac{0.2}{R_{IFB} (\Omega)} \quad (5)$$

For example, if R_{ISET} is 80k Ω , then the V_{REF_FULL} is 100mV. For improved accuracy, a 40k Ω to 80k Ω R_{ISET} is recommended to achieve a 200mV to 100mV V_{REF_FULL} .

Setting the Feedback Resistor

The power loss of the sensing resistor (P_{LOSS_RIFB}) can be calculated with Equation (6):

$$P_{LOSS_RIFB} = \frac{V_{REF_FULL}^2}{R_{IFB} (\Omega)} \quad (6)$$

To guarantee a current reference, the nominated power rating of P_{LOSS_RIFB} is recommended to be twice the calculated power loss with a minimum 1% accuracy resistor.

Setting the Switching Frequency

A higher f_{SW} results in smaller current ripple; however, the MOSFETs' switching loss is also

higher. Therefore, a tradeoff is required for the design. f_{FREQ} can be calculated with Equation (7):

$$f_{FREQ} = \frac{22500}{R_{FREQ} (k\Omega)} \quad (7)$$

Since the power loss of this resistor is small, a 0603 or 0402 resistor size is sufficient.

Selecting the Compensation Loop

The loop compensation components stabilize the closed loop and achieve improved transient response (see Figure 5).

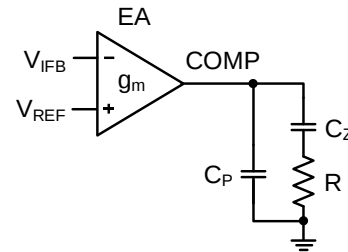


Figure 5: Compensation Loop

The transfer function of loop compensation from the EA input to the EA output (G_C) can be calculated with Equation (8):

$$G_C(s) = \frac{g_m}{(C_Z + C_P)s} \frac{(1 + sRC_Z)}{(1 + sR \frac{C_Z C_P}{C_Z + C_P})} \quad (8)$$

Where g_m is the EA's transconductance.

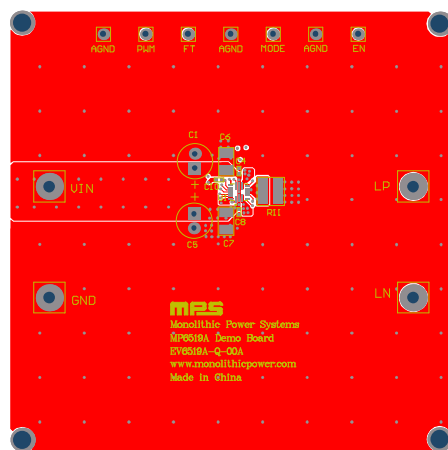
The transfer function's zero point is comprised of R and the zero point (C_Z). The pole point is comprised of R and C_Z in parallel with the polar point (C_P).

Typically, for an inductive load with resistance, the compensation zero can be set as the load pole, which is comprised of the load inductance (L) and its resistance. The compensation pole point is typically set to about f_{SW} to eliminate high-frequency noise. After the zero and pole point of the compensation is fixed, R can be used to increase the loop bandwidth. 1/10 to 1/5 of f_{SW} can be set as the closed-loop bandwidth to achieve optimal system response.

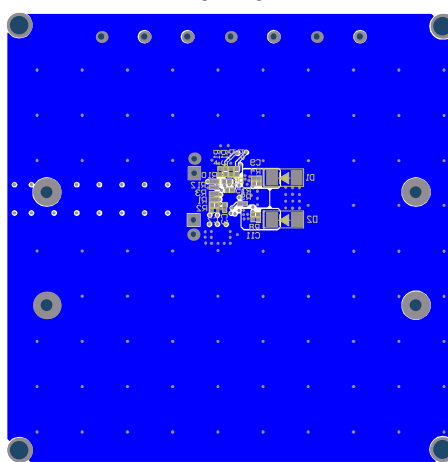
PCB Layout Guidelines

Efficient PCB layout is critical for stable operation. For the best results, refer to Figure 6 and follow the guidelines below:

1. Place C_{IN} close to the VIN pin.
2. Use wider copper for the input, output, and ground-connecting wire to improve thermal performance.
3. Place as many ground vias near the output capacitor (C_{OUT}) and C_{IN} as possible to improve thermal performance.
4. Keep the IFB feedback signal far away from noise sources.



Top Layer



Bottom Layer

Figure 6: Recommended PCB Layout

TYPICAL APPLICATION CIRCUIT

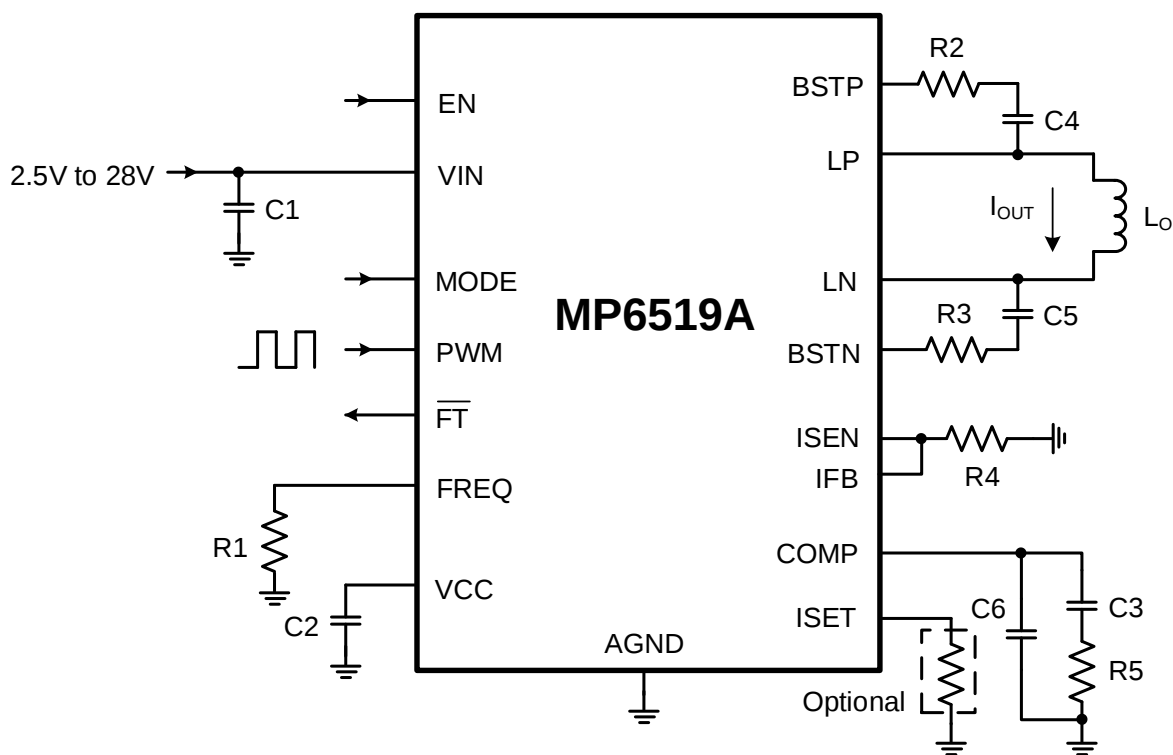
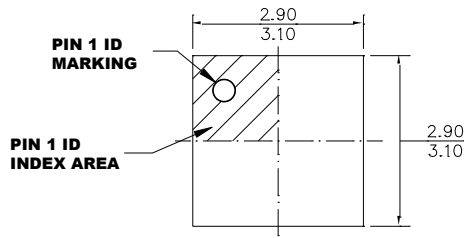


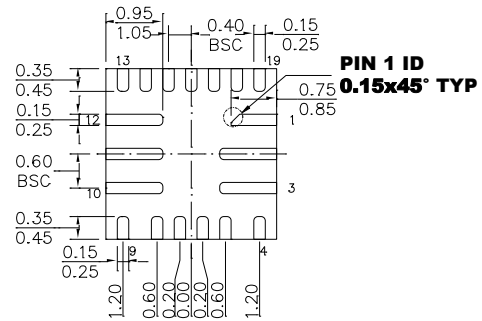
Figure 7: Typical Application Circuit

PACKAGE INFORMATION

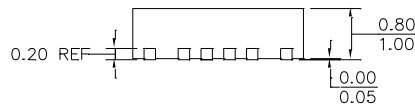
QFN-19 (3mmx3mm)



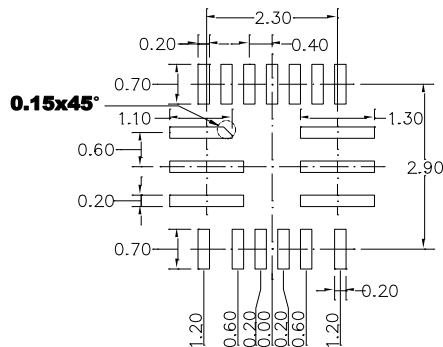
TOP VIEW



BOTTOM VIEW



SIDE VIEW

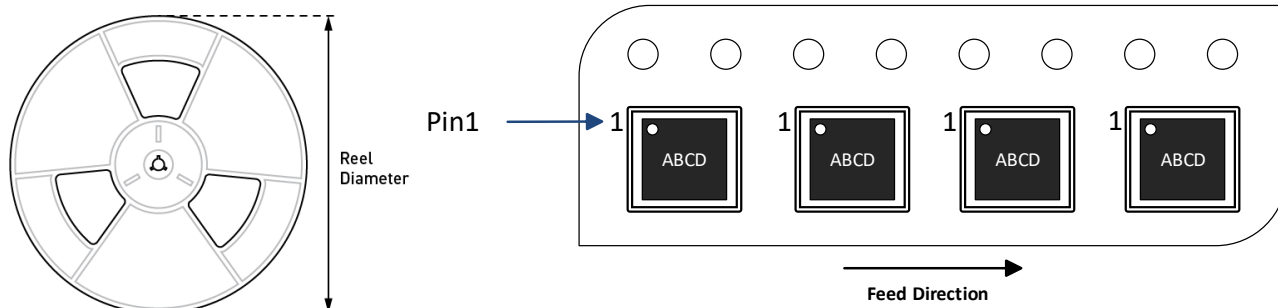


RECOMMENDED LAND PATTERN

NOTE:

- 1) LAND PATTERNS OF PIN2,3,10,11 AND 12 HAVE THE SAME SHAPE.
- 2) ALL DIMENSIONS ARE IN MILLIMETERS.
- 3) LEAD COPLANARITY SHALL BE 0.10 MILLIMETERS MAX.
- 4) JEDEC REFERENCE IS MO-220.
- 5) DRAWING IS NOT TO SCALE.

CARRIER INFORMATION



Part Number	Package Description	Quantity/ Reel	Quantity/ Tube	Quantity/ Tray	Reel Diameter	Carrier Tape Width	Carrier Tape Pitch
MP6519AGQ	QFN-19 (3mmx3mm)	5000	N/A	N/A	13in	12mm	8mm



REVISION HISTORY

Revision #	Revision Date	Description	Pages Updated
1.0	7/15/2024	Initial Release	-

Notice: The information in this document is subject to change without notice. Please contact MPS for current specifications. Users should warrant and guarantee that third-party Intellectual Property rights are not infringed upon when integrating MPS products into any application. MPS will not assume any legal responsibility for any said applications.