DESCRIPTION
The HF500-7 is a fixed-frequency, current-mode regulator with built-in slope compensation. The HF500-7 combines a 700V MOSFET and a full-featured controller into one chip for a low-power, offline, flyback, switch-mode power supply. At medium and heavy loads, the regulator works in a fixed frequency with frequency jittering, which helps spread energy out in a conducted mode. During a light-load condition, the regulator freezes the peak current and reduces its switching frequency to \( f_{\text{OSC(min)}} \) to offer excellent efficiency at light load. At very light loads, the regulator enters burst mode to achieve low standby power consumption.

Full protection features include thermal shutdown, brown-in and brown-out, VCC under-voltage lockout (UVLO), overload protection (OLP), short-circuit protection (SCP), input and output over-voltage protection (OVP), and over-temperature protection (OTP).

The HF500-7 features timer-based fault detection and over-power compensation to ensure that the overload protection point is independent of the input voltage. The HF500-7 can also be self-supplied without any auxiliary winding to save BOM cost.

The HF500-7 is available in a SOIC8-7B package.

<table>
<thead>
<tr>
<th>Vcc</th>
<th>Maximum Output Power (^{(1)})</th>
</tr>
</thead>
<tbody>
<tr>
<td>external supplied</td>
<td>Adapter (^{(2)})</td>
</tr>
<tr>
<td>230Vac±15%</td>
<td>85Vac–265Vac</td>
</tr>
<tr>
<td>6.5W</td>
<td>7W</td>
</tr>
<tr>
<td>115Vac±15%</td>
<td>230Vac±15%</td>
</tr>
<tr>
<td>self-supplied</td>
<td>5W</td>
</tr>
</tbody>
</table>

NOTES:
1) The junction temperature can limit the maximum output power.
2) Maximum continuous power in a non-ventilated enclosed adapter measured at 50° C ambient temperature.
3) Maximum continuous power in an open frame design at 50°C ambient temperature.
TYPICAL APPLICATION

VCC Supplied by Auxiliary Winding and Adopted Brown-In/-Out Function

VCC Self-Supplied and Disabled Brown-In/-Out Function
**ORDERING INFORMATION**

<table>
<thead>
<tr>
<th>Part Number*</th>
<th>Package</th>
<th>Top Marking</th>
</tr>
</thead>
<tbody>
<tr>
<td>HF500GS-7</td>
<td>SOIC8-7B</td>
<td>See Below</td>
</tr>
</tbody>
</table>

* For Tape & Reel, add suffix –Z (e.g. HF500GS-7–Z)

**TOP MARKING**

HF500-7, LLLLLLLLL, MPSYWW

HF500-7: Part number
LLLLLLLL: Lot number
MPS: MPS prefix
Y: Year code
WW: Week code

**PACKAGE REFERENCE**

TOP VIEW

![Diagram of SOIC8-7B package](image-url)
ABSOLUTE MAXIMUM RATINGS (1)
DRAIN breakdown voltage ........ -0.3V to 700V
VCC to GND ................................ -0.3V to 30V
FB, TIMER, SOURCE, B/O to GND ..............
........................................................................... -0.3V to 7V
Continuous power dissipation (T_A = +25°C) (2)
........................................................................... 1.5W
Junction temperature .............................. 150°C
Lead temperature ............................... 260°C
Storage temperature ............... -60°C to +150°C
ESD capability human body model (all pins except DRAIN) ................................. 4.0kV
ESD capability machine model ........... 200V

Recommended Operating Conditions (3)
Operating junction temp. (T_J) ........ -40°C to +125°C
Operating VCC range ....................... 12.5V to 24V

Thermal Resistance (4) θ_JA θ_JC
SOIC8-7B ........................................ 85 ........ 40 °C/W

NOTES:
1) Exceeding these ratings may damage the device.
2) The maximum allowable power dissipation is a function of the maximum junction temperature T_J (MAX), the junction-to-ambient thermal resistance θ_JA, and the ambient temperature T_A. The maximum allowable continuous power dissipation at any ambient temperature is calculated by P_D (MAX) = (T_J (MAX) - T_A) / θ_JA. Exceeding the maximum allowable power dissipation produces an excessive die temperature, causing the regulator to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
3) The device is not guaranteed to function outside of its operating conditions.
4) Measured on JESD51-7, 4-layer PCB.
**ELECTRICAL CHARACTERISTICS** (5)
For typical value, VCC = 16V, TJ = -40°C to 125°C, unless otherwise noted.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Conditions</th>
<th>Min</th>
<th>Typ</th>
<th>Max</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Start-Up Current Source (DRAIN)</strong></td>
<td></td>
<td></td>
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</tr>
<tr>
<td>Supply current from DRAIN</td>
<td>IDrain_0</td>
<td>VCC = 0V, VDRAIN = 120V/400V</td>
<td>1.4</td>
<td>3.6</td>
<td>6.2</td>
<td>mA</td>
</tr>
<tr>
<td></td>
<td>IDrain_11</td>
<td>VCC = 11V, VDRAIN = 120V/400V</td>
<td>1.4</td>
<td>5</td>
<td>7.8</td>
<td>mA</td>
</tr>
<tr>
<td>Leakage current from DRAIN</td>
<td>ILK</td>
<td>VCC = 10V, VDRAIN = 400V</td>
<td>4.5</td>
<td>10.5</td>
<td>µA</td>
<td></td>
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<tr>
<td>Breakdown voltage</td>
<td>VBR</td>
<td>TJ = 25°C</td>
<td>700</td>
<td></td>
<td></td>
<td>V</td>
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<tr>
<td><strong>Internal MOSFET (DRAIN)</strong></td>
<td></td>
<td></td>
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<tr>
<td>On-state resistance</td>
<td>RDS_ON</td>
<td>VCC = 10.5V, ID = 0.1A, TJ = 25°C</td>
<td>12</td>
<td>15.5</td>
<td></td>
<td>Ω</td>
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<tr>
<td><strong>Supply Voltage Management (VCC)</strong></td>
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<td>VCC level (increasing) where the</td>
<td>VCCOFF</td>
<td></td>
<td>11</td>
<td>12</td>
<td>13</td>
<td>V</td>
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<tr>
<td>internal regulator stops</td>
<td></td>
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<td>VCC level (decreasing) where the</td>
<td>VCCUVLO</td>
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<td>6</td>
<td>7</td>
<td>8</td>
<td>V</td>
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<tr>
<td>the IC shuts down and the</td>
<td></td>
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<tr>
<td>internal regulator turns on</td>
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<tr>
<td>VCC level (decreasing) where the</td>
<td>VCCON</td>
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<td>10.4</td>
<td>11.5</td>
<td>12.6</td>
<td>V</td>
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<tr>
<td>the internal regulator turns on</td>
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<tr>
<td>VCC regulator on and off</td>
<td>VHY</td>
<td></td>
<td>400</td>
<td>500</td>
<td></td>
<td>mV</td>
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<tr>
<td>hysteresis</td>
<td></td>
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<td>VCC UVLO hysteresis</td>
<td>VCCOFF -</td>
<td></td>
<td>4</td>
<td>4.8</td>
<td></td>
<td>V</td>
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<td>VCCUVLO</td>
<td>VCCUVLO</td>
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<tr>
<td>VCC recharge level when protection</td>
<td>VCCPRO</td>
<td></td>
<td>4.7</td>
<td>5.3</td>
<td>5.9</td>
<td>V</td>
</tr>
<tr>
<td>occurs</td>
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<tr>
<td>VCC decreasing level where the</td>
<td>VCCLATCH</td>
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<td>2.5</td>
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<td></td>
<td>V</td>
</tr>
<tr>
<td>latch-off phase ends</td>
<td></td>
<td></td>
<td></td>
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<tr>
<td>Internal IC consumption</td>
<td>ICC</td>
<td>VFB = 3V, VCC = 12V</td>
<td>0.9</td>
<td>1.2</td>
<td></td>
<td>mA</td>
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<tr>
<td>Internal IC consumption, latch-off</td>
<td>ICCLATCH</td>
<td>VCC = 12V, TJ = 25°C</td>
<td>700</td>
<td>900</td>
<td></td>
<td>µA</td>
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<tr>
<td>phase</td>
<td></td>
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<tr>
<td>Voltage on VCC (upper limit) where</td>
<td>VDVP</td>
<td>VCC = 12V, TJ = 25°C</td>
<td>25</td>
<td>27</td>
<td>29</td>
<td>V</td>
</tr>
<tr>
<td>the regulator latches off (OVP)</td>
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<tr>
<td>Blanking duration on the OVP comparator</td>
<td>TOVP</td>
<td></td>
<td>60</td>
<td></td>
<td></td>
<td>ms</td>
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<td><strong>Oscillator</strong></td>
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<tr>
<td>Oscillator frequency</td>
<td>fOSC</td>
<td>VFB &gt; 1.85V, TJ = 25°C</td>
<td>62</td>
<td>65</td>
<td>68</td>
<td>kHz</td>
</tr>
<tr>
<td>Frequency jittering amplitude in</td>
<td>AJitter</td>
<td>VFB &gt; 1.85V, TJ = 25°C</td>
<td>±5</td>
<td>±6.5</td>
<td>±8</td>
<td>%</td>
</tr>
<tr>
<td>percentage of fOSC</td>
<td></td>
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<tr>
<td>Frequency jittering entry level</td>
<td>VFB_JITTER</td>
<td></td>
<td>1.95</td>
<td></td>
<td></td>
<td>V</td>
</tr>
<tr>
<td>Frequency jittering modulation period</td>
<td>Tjitter</td>
<td>CTIMER = 47nF</td>
<td>3.7</td>
<td></td>
<td></td>
<td>ms</td>
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</tbody>
</table>
### ELECTRICAL CHARACTERISTICS (5) (continued)

For typical value, VCC = 16V, TJ = -40°C to 125°C, unless otherwise noted.

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<th>Min</th>
<th>Typ</th>
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<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>Protections (B/O)</td>
<td></td>
<td></td>
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<tr>
<td>Brown-in threshold voltage on B/O</td>
<td>V_{B/O_IN}</td>
<td>V_B/O increasing</td>
<td>0.95</td>
<td>1</td>
<td>1.05</td>
<td>V</td>
</tr>
<tr>
<td>Brownout threshold voltage on B/O</td>
<td>V_{B/O_OUT}</td>
<td>V_B/O decreasing</td>
<td>0.85</td>
<td>0.9</td>
<td>0.95</td>
<td>V</td>
</tr>
<tr>
<td>Brown-in/-out hysteresis</td>
<td>ΔV_{B/O}</td>
<td></td>
<td>0.065</td>
<td>0.1</td>
<td>0.14</td>
<td>V</td>
</tr>
<tr>
<td>Timer duration for line cycle dropout</td>
<td>T_{B/O}</td>
<td>CTIMER = 47nF</td>
<td>34</td>
<td>55</td>
<td></td>
<td>ms</td>
</tr>
<tr>
<td>Input OVP threshold on B/O</td>
<td>OVP_{B/O}</td>
<td></td>
<td>4.2</td>
<td>4.5</td>
<td>4.8</td>
<td>V</td>
</tr>
<tr>
<td>Input OVP delay time</td>
<td>T_{OVBP/B}</td>
<td></td>
<td>5.4</td>
<td>6</td>
<td>6.6</td>
<td>V</td>
</tr>
<tr>
<td>Voltage on B/O to disable B/O and input OVP function</td>
<td>V_{DIS}</td>
<td></td>
<td>7</td>
<td></td>
<td></td>
<td>V</td>
</tr>
<tr>
<td>Clamp voltage on B/O</td>
<td>V_{B/O_Cla}</td>
<td></td>
<td>1.2</td>
<td></td>
<td></td>
<td>MΩ</td>
</tr>
<tr>
<td>Current Sense (SOURCE)</td>
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<tr>
<td>Current-limit point</td>
<td>V_{ILIM}</td>
<td></td>
<td>0.93</td>
<td>1</td>
<td>1.07</td>
<td>V</td>
</tr>
<tr>
<td>Short-circuit protection point</td>
<td>V_{SCP}</td>
<td></td>
<td>1.3</td>
<td>1.5</td>
<td>1.7</td>
<td>V</td>
</tr>
<tr>
<td>Current limitation during frequency foldback</td>
<td>V_{FOLD}</td>
<td>V_FB = 1.85V</td>
<td>0.63</td>
<td>0.68</td>
<td>0.73</td>
<td>V</td>
</tr>
<tr>
<td>Current limitation when entering burst</td>
<td>V_{IBURL}</td>
<td>V_FB = 0.7V</td>
<td>0.18</td>
<td></td>
<td></td>
<td>V</td>
</tr>
<tr>
<td>Current limitation when exiting burst</td>
<td>V_{IBURH}</td>
<td>V_FB = 0.8V</td>
<td>0.23</td>
<td></td>
<td></td>
<td>V</td>
</tr>
<tr>
<td>Leading-edge blanking for V_{ILIM}</td>
<td>T_{LEB1}</td>
<td></td>
<td>350</td>
<td></td>
<td></td>
<td>ns</td>
</tr>
<tr>
<td>Leading-edge blanking for V_{SCP}</td>
<td>T_{LEB2}</td>
<td></td>
<td>270</td>
<td></td>
<td></td>
<td>ns</td>
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<tr>
<td>Slope of the compensation ramp</td>
<td>S_{RAMP}</td>
<td></td>
<td>18</td>
<td>25</td>
<td>31</td>
<td>mV/μs</td>
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<tr>
<td>Feedback (FB)</td>
<td></td>
<td></td>
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<td></td>
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<tr>
<td>Internal pull-up resistor</td>
<td>R_{FB}</td>
<td>T_J = 25°C</td>
<td>12</td>
<td>13.5</td>
<td>15</td>
<td>kΩ</td>
</tr>
<tr>
<td>Internal pull-up voltage</td>
<td>V_{DD}</td>
<td></td>
<td>4.3</td>
<td></td>
<td></td>
<td>V</td>
</tr>
<tr>
<td>V_FB to internal current-set point division ratio</td>
<td>K_{FB1}</td>
<td>V_FB = 2V</td>
<td>2.5</td>
<td>2.8</td>
<td>3.1</td>
<td></td>
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<tr>
<td>V_FB to current-set point division ratio</td>
<td>K_{FB2}</td>
<td>V_FB = 3V</td>
<td>2.8</td>
<td>3.1</td>
<td>3.4</td>
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<tr>
<td>FB level (decreasing) where the regulator enters burst mode</td>
<td>V_{BURL}</td>
<td></td>
<td>0.63</td>
<td>0.7</td>
<td>0.77</td>
<td>V</td>
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<tr>
<td>FB level (increasing) where the regulator exits burst mode</td>
<td>V_{BURH}</td>
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<td>0.72</td>
<td>0.8</td>
<td>0.88</td>
<td>V</td>
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<tr>
<td>Overload Protection (FB)</td>
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<tr>
<td>FB level where the regulator enters OLP after a dedicated time</td>
<td>V_{OLP}</td>
<td></td>
<td>3.7</td>
<td></td>
<td></td>
<td>V</td>
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<tr>
<td>Time duration before OLP when FB reaches the protection point</td>
<td>T_{OLP}</td>
<td>CTIMER = 47nF</td>
<td>32</td>
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<td>ms</td>
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</table>
### ELECTRICAL CHARACTERISTICS (5) *(continued)*

For typical value, VCC = 16V, T_J = -40°C to 125°C, unless otherwise noted.

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<th>Max</th>
<th>Unit</th>
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</thead>
<tbody>
<tr>
<td>Over-Power Compensation (B/O)</td>
<td>V_{OPC}</td>
<td>V_{BO} = 1.1V, V_{FB} = 2.5V,</td>
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<td></td>
<td></td>
<td>mV</td>
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<tr>
<td>Compensation voltage</td>
<td></td>
<td>T_J = 25°C</td>
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</tr>
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<td></td>
<td></td>
<td>V_{BO} = 1.3V, V_{FB} = 2.5V,</td>
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<tr>
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<td>T_J = 25°C</td>
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<td></td>
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<td>V_{BO} = 2.9V, V_{FB} = 2.5V,</td>
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<td>V_{BO} = 3.5V, V_{FB} = 2.5V,</td>
<td>205</td>
<td>270</td>
<td>335</td>
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<td>T_J = 25°C</td>
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<td>V_{BO} &gt; V_{DIS}, T_J = 25°C</td>
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<td>FB voltage (lower limit) when</td>
<td>V_{OPC(OFF)}</td>
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<td>0.55</td>
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<td>V</td>
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<tr>
<td>compensation is removed</td>
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<tr>
<td>FB voltage (upper limit) when</td>
<td>V_{OPC(ON)}</td>
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<td>2.5</td>
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<td></td>
<td>V</td>
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<tr>
<td>compensation is fully applied</td>
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<tr>
<td>Frequency Foldback</td>
<td>V_{FB(FOLD)}</td>
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<td></td>
<td>V</td>
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<tr>
<td>FB voltage (lower threshold) when</td>
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</tr>
<tr>
<td>frequency foldback starts</td>
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<td>Minimum switching frequency</td>
<td>f_{OSC(min)}</td>
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<td>25</td>
<td>30</td>
<td>kHz</td>
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<td>T_J = 25°C</td>
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<td></td>
<td></td>
</tr>
<tr>
<td>FB voltage (lower threshold) when</td>
<td>V_{FB(FOLDE)}</td>
<td></td>
<td>1</td>
<td></td>
<td></td>
<td>V</td>
</tr>
<tr>
<td>frequency foldback ends</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Latch-Off Input (Integration in TIMER)</td>
<td>V_{TIMMER(LATCH)}</td>
<td></td>
<td>0.7</td>
<td>1</td>
<td>1.2</td>
<td>V</td>
</tr>
<tr>
<td>Lower threshold when the regulator is</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>latched</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Blanking duration on latch detection</td>
<td>T_{LATCH}</td>
<td></td>
<td>42</td>
<td></td>
<td></td>
<td>μs</td>
</tr>
<tr>
<td>Thermal Shutdown</td>
<td>T_{TSD}</td>
<td></td>
<td>150</td>
<td></td>
<td></td>
<td>°C</td>
</tr>
<tr>
<td>Thermal shutdown threshold</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Thermal shutdown hysteresis</td>
<td>T_{TSD(HYS)}</td>
<td></td>
<td>25</td>
<td></td>
<td></td>
<td>°C</td>
</tr>
</tbody>
</table>
TYPICAL CHARACTERISTICS

LKG_Drain_400V vs. Temperature Chart

BV_Drain vs. Temperature Chart

I_DRAIN_0 vs. Temperature Chart

I_DRAIN_11 vs. Temperature Chart

V_OPC4 vs. Temperature Chart

VCC_OFF vs. Temperature Chart

VCC_UVLO vs. Temperature Chart

VCC_OVP vs. Temperature Chart

VCC_Latch vs. Temperature Chart
TYPICAL CHARACTERISTICS (continued)

- **VCC_PRO vs. Temperature**
- **VBO_IN vs. Temperature**
- **VBO_OUT vs. Temperature**
- **BO_OVP vs. Temperature**
- **VDIS vs. Temperature**
- **V_BURL vs. Temperature**
- **V_BURH vs. Temperature**
- **V_IBURL vs. Temperature**
- **V_IBURH vs. Temperature**
TYPICAL CHARACTERISTICS (continued)

- **VFB_OLP vs. Temperature**
  - Graph showing the variation of VFB_OLP with temperature.

- **VCS_MAX vs. Temperature**
  - Graph showing the variation of VCS_MAX with temperature.

- **V_SCP vs. Temperature**
  - Graph showing the variation of V_SCP with temperature.

- **F_OSC vs. Temperature**
  - Graph showing the variation of F_OSC with temperature.

- **F_OSC_MIN vs. Temperature**
  - Graph showing the variation of F_OSC_MIN with temperature.

- **Slope_Comp vs. Temperature**
  - Graph showing the variation of Slope_Comp with temperature.

- **T_LEB1 vs. Temperature**
  - Graph showing the variation of T_LEB1 with temperature.

- **T_LEB2_LOW vs. Temperature**
  - Graph showing the variation of T_LEB2_LOW with temperature.

- **RDS_ON vs. Temperature**
  - Graph showing the variation of RDS_ON with temperature.
TYPICAL PERFORMANCE CHARACTERISTICS

\(V_{\text{IN}} = 230V_{\text{AC}}, \ V_{\text{OUT1}}/V_{\text{OUT2}} = 12V/5V, \ I_{\text{OUT1}}/I_{\text{OUT2}} = 0.3A/0.3A,\) unless otherwise noted.

Input Power On

\[\text{Input Power Off}\]

Output Ripple

SCP Power On

SCP Power Off

SCP Release

OLP Entry, No Load

OLP Entry, Full Load

Brown In, Full Load
TYPICAL PERFORMANCE CHARACTERISTICS (continued)

\( V_{\text{IN}} = 230V_{\text{AC}}, \) \( V_{\text{OUT1}}/V_{\text{OUT2}} = 12V/5V, \) \( I_{\text{OUT1}}/I_{\text{OUT2}} = 0.3A/0.3A, \) unless otherwise noted.

**Brown Out, Full Load**

- \( V_{\text{DS}} \)
- \( 100V/\text{div.} \)
- \( V_{\text{CC}} \)
- \( 10V/\text{div.} \)
- \( 5V/\text{div.} \)
- \( V_{\text{BO}} \)
- \( 500mV/\text{div.} \)

**OVP Entry, No Load**

- \( V_{\text{DS}} \)
- \( 200V/\text{div.} \)
- \( V_{\text{CC}} \)
- \( 10V/\text{div.} \)

**OVP Recovery, No Load**

- \( V_{\text{DS}} \)
- \( 200V/\text{div.} \)
- \( V_{\text{CC}} \)
- \( 10V/\text{div.} \)

**OVP Power On, No Load**

- \( V_{\text{DS}} \)
- \( 200V/\text{div.} \)
- \( V_{\text{CC}} \)
- \( 10V/\text{div.} \)

**OTP Entry**

- \( V_{\text{DS}} \)
- \( 100V/\text{div.} \)
- \( V_{\text{CC}} \)
- \( 10V/\text{div.} \)

**OTP Recovery**

- \( V_{\text{DS}} \)
- \( 100V/\text{div.} \)
- \( V_{\text{CC}} \)
- \( 10V/\text{div.} \)

**Stress**

- \( V_{\text{DS}} \)
- \( 100V/\text{div.} \)

**Conducted EMI, L**

- Magnetic Field Strength

**Conducted EMI, N**

- Magnetic Field Strength
### PIN FUNCTIONS

<table>
<thead>
<tr>
<th>Pin #</th>
<th>Name</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>FB</td>
<td>Feedback. A pull-down optocoupler controls the output regulation.</td>
</tr>
<tr>
<td>2</td>
<td>VCC</td>
<td>Power supply of the IC. VCC enters over-voltage protection (OVP) if the VCC voltage rises above $V_{OVP}$.</td>
</tr>
<tr>
<td>4</td>
<td>DRAIN</td>
<td>Drain of the internal MOSFET. DRAIN is the input for the start-up, high-voltage current source.</td>
</tr>
<tr>
<td>5</td>
<td>SOURCE</td>
<td>Source of the internal MOSFET. SOURCE is the input of the primary current-sense signal.</td>
</tr>
<tr>
<td>6</td>
<td>GND</td>
<td>Ground.</td>
</tr>
<tr>
<td>7</td>
<td>B/O</td>
<td>Brown-in/-out, input OVP, and over-power compensation detection. Brown-in/-out, input OVP, and over-power compensation are achieved by detecting the voltage on B/O. All functions are disabled when B/O is pulled higher than $V_{DIS}$.</td>
</tr>
<tr>
<td>8</td>
<td>TIMER</td>
<td>Combined soft start, frequency jittering, and timer functions for overload protection (OLP) and brown-out protection. The IC is latched by pulling TIMER down. TIMER allows for external OVP and over-temperature protection (OTP) detection.</td>
</tr>
</tbody>
</table>
Figure 1: Functional Block Diagram
OPERATION

The HF500–7 is a fixed-frequency, current-mode regulator with built-in slope compensation that incorporates all of the necessary features to build a reliable switch-mode power supply. In light-load conditions, the regulator freezes the peak current and reduces its switching frequency to 25kHz to minimize switching loss. When the output power falls below a given level, the regulator enters burst mode. The HF500–7 uses frequency jittering to improve EMI performance.

Fixed Frequency with Jittering

Frequency jittering reduces EMI by spreading out the energy (see Figure 2).

![Figure 2: Frequency Jitter Circuit](image)

An internal capacitor is charged with a controlled current source, which is fixed when FB is greater than 2V, and its voltage is compared with the TIMER voltage (V_TIMER). V_TIMER is a triangular wave between 2.8V and 3.2V with a charging/discharging current (see Figure 3). The switching frequency can be calculated using Equation (1):

$$f_s = \frac{1 \cdot 10^6}{5.28 \cdot V_{\text{TIMER}} / V + 0.2} \text{Hz}$$

(1)

T_jitter can be calculated using Equation (2):

$$T_{\text{jitter}} = 8 \cdot C_{\text{TIMER}} / nF \cdot 10^{-5} \text{s}$$

(2)

Figure 3: Frequency Jittering

Frequency Foldback

To achieve high efficiency during all load conditions, the HF500–7 implements frequency foldback during light-load conditions.

When the load decreases to a given level, the regulator freezes the V_FOLD peak current and reduces the charging current, dropping its switching frequency down to 25kHz and reducing switching loss. If the load continues to decrease, the peak current decreases with a 25kHz fixed frequency to avoid audible noise. Figure 4 shows the frequency and peak current vs. FB.

![Figure 4: Frequency and Peak Current vs. FB](image)

Current-Mode Operation with Slope Compensation

The primary peak current is controlled by the FB voltage (V_FB). When the peak current reaches the level determined by FB, the MOSFET turns off. The regulator can also operate in continuous conduction mode (CCM) with a wide input voltage range. Its internal synchronous slope compensation (S_RAMP) helps avoid subharmonic oscillation when the duty cycle is larger than 50% at CCM.
High-Voltage Start-Up Current Source

Initially, the IC is self-supplied by the internal high-voltage current source, which is drawn from DRAIN. The IC turns off the current source once VCC reaches VCCOFF. If VCC falls below VCCON, the high-voltage current source turns on again.

The lower threshold of VCC is pulled down from VCCUVLO to VCCPRO when a fault condition occurs, such as overload protection (OLP), short-circuit protection (SCP), brown-out, over-voltage protection (OVP), and over-temperature protection (OTP), etc.

Self-Power Supply

The IC can be self-supplied by the internal high-voltage current source. The IC starts switching and the internal high-voltage current source turns off once the VCC voltage reaches VCCOFF (typically 12V). Then the VCC voltage decreases. The internal high-voltage current source turns on again to charge the external VCC capacitor when the VCC voltage decreases below VCCON (typically 11.5V) (see Figure 5). A small capacitor (several μF) is enough to hold the VCC voltage. The self-supply function can lower the total BOM cost by removing auxiliary winding and decreasing the capacitance of the VCC capacitor.

![Figure 5: Self-Power Supply](image)

Self-power supply leads to higher no-load power consumption. If tough no-load power consumption performance is required, the self-supply function should be disabled.

Soft Start (SS)

To reduce the stress on the power components and smoothly establish the output voltage, the TIMER voltage increases from 1V to 1.75V with a 1/4 charge current during normal operation during every start-up. The TIMER voltage increases the peak current from 0.25V to 1V gradually. The switching frequency also increases gradually. Figure 6 shows the typical waveform of a soft start.

![Figure 6: Soft Start](image)

The start-up duration can be adjusted by the capacitor connected to TIMER. The TIMER capacitor determines the start-up duration, shown in Equation (3):

\[
T_{\text{Soft-start}} = 0.3 \cdot C_{\text{TIMER}} / \text{nF} \cdot 10^{-3} \text{s} \quad (3)
\]

Burst Operation

The HF500-7 uses burst-mode operation to minimize the power dissipation in no-load or light-load conditions. As the load decreases, \(V_{FB}\) decreases. The IC stops the switching cycle when \(V_{FB}\) drops below the lower threshold (\(V_{BURL}\)). \(V_{FB}\) increases again once the output voltage drops, and switching resumes once \(V_{FB}\) exceeds the threshold (\(V_{BURH}\)). \(V_{FB}\) then falls and rises repeatedly. Burst-mode operation alternately enables and disables the switching cycle of the MOSFET, thereby reducing switching loss at no-load or light-load conditions.

Over-Power Compensation (OPC)

An offset voltage proportional to the B/O voltage is added to the sensing voltage. The B/O voltage is proportional to the input voltage. Figure 7 shows the compensation in relation to the voltage on FB and B/O. The over-power compensation (OPC) voltage \(V_{OPC}\) can be calculated using Equation (4):

\[
V_{OPC} = 0.094 \cdot (V_{B/O} - 1.1V) \quad (4)
\]
Timer-Based Overload Protection (OLP)

If the switching frequency is fixed in a flyback converter, the maximum output power is limited by the peak current. When the output consumes more than the limited power, the output voltage drops below the set value. The current flowing through the primary and secondary optocoupler is reduced, and \( V_{FB} \) is pulled high (see Figure 8).

![Figure 8: Overload Protection Block](image)

FB rising higher than \( V_{OLP} \) is considered to be an error flag and causes the timer to start counting the rising edge of \( V_O \). When the error flag is removed, the timer resets. When the timer completes after it has counted to 16, the HR500-7 enters OLP. This timer duration does not trigger the OLP function when the power supply is starting up or during a load transition phase (see Figure 9).

![Figure 9: Overload Protection Function](image)

Input Brown-Out and Input OVP

The input brown-out and input OVP are performed by B/O. If the B/O voltage is higher than \( V_{B/O\_IN} \) during the input voltage rising period, the IC begins operating. If the B/O voltage is lower than \( V_{B/O\_OUT} \) for \( T_{B/O} \) (\( C_{TIMER} = 47nF \)), the IC stops operation. If the voltage on B/O is higher than OVP\_B/O for \( T_{OVP\_B/O} \), the IC stops operating, achieving input OVP. If the voltage on B/O is higher than \( V_{DIS} \), input brown-out and input OVP are disabled. To simplify the external circuit, connect B/O to VCC through a resistor if input brown-out, over-power compensation, and input OVP are not needed.

Short-Circuit Protection (SCP)

The HF500-7 features a short-circuit protection (SCP) that senses the SOURCE voltage and stops switching if \( V_{SOURCE} \) reaches \( V_{SCP} \) after a reduced leading-edge blanking time (\( T_{LEB2} \)). Once the fault disappears, the power supply resumes operation.

Thermal Shutdown

The HF500-7 uses thermal shutdown to turn off the switching cycle when the inner temperature exceeds \( T_{OTP} \). Once the inner temperature drops below \( T_{OTP}(\_HS) \), the power supply resumes operation. During thermal shutdown, the VCC UVLO lower threshold is pulled down from \( V_{CC\_UVLO} \) to \( V_{CC\_PRO} \).

Vcc Over-Voltage Protection (OVP)

The HF500-7 enters a latched fault condition if the VCC voltage rises above \( V_{OVP} \) for \( T_{OVP} \). The regulator remains fully latched until VCC drops below \( V_{CC\_LATCH} \), such as when the power supply is unplugged from the main input and plugged back in. Usually, this situation occurs when the optocoupler fails, resulting in the loss of the output voltage regulation.

TIMER Protection

The HF500-7 is latched off by pulling TIMER below \( V_{TIMER(\_LATCH)} \) for \( T_{LATCH} \). This allows TIMER to be used for external OVP and OTP functions by adding an external compact circuit.
Leading-Edge Blanking (LEB)

An internal leading-edge blanking (LEB) unit containing two LEB times is placed between SOURCE and the current comparator input to avoid premature switching pulse termination due to parasitic capacitances. During the blanking time, the current comparator is disabled and cannot turn off the external MOSFET (see Figure 10).

![Leading-Edge Blanking Diagram](image)

Figure 10: Leading-Edge Blanking
APPLICATION INFORMATION

VCC Capacitor Selection

When the input voltage is supplied, the VCC capacitor is charged up by the IC internal high-voltage current source. Due to the self-supply function, the start-up period is not affected by the VCC capacitor selection. The main concern is that the self-supply function should always be disabled during burst mode if VCC is supplied by the auxiliary winding. The value for the VCC capacitor can be estimated with Equation (5):

\[ C_{VCC} > \frac{I_{CC} \cdot T_{burst}}{V_{CC \text{ OFF}} - V_{CC \text{ ON}}} \]  

(5)

Where \( I_{CC} \) is the internal consumption, and \( T_{burst} \) is the interval during the burst period.

Primary-Side Inductor Design (\( L_m \))

The HF500-7 uses an internal slope compensation to support CCM when the duty cycle exceeds 50%. Set a ratio (\( K_P \)) of the primary inductor’s ripple current amplitude vs. the peak current value to \( 0 < K_P \leq 1 \), where \( K_P = 1 \) for discontinuous conduction mode (DCM) (see Figure 11). A larger inductor leads to a smaller \( K_P \), which reduces the RMS current but increases transformer size. An optimal \( K_P \) value is between 0.7 and 0.8 for the universal input range and under CrCM or under DCM for the 230V\(_{AC}\) input range.

![Figure 11: Typical Primary Current Waveform](image)

The input power (\( P_{in} \)) at the minimum input can be estimated with Equation (6):

\[ P_{in} = \frac{V_O \cdot I_O}{\eta} \]  

(6)

Where \( V_O \) is the output voltage, \( I_O \) is the rated output current, and \( \eta \) is the estimated efficiency, typically between 0.75 and 0.85 depending on the input range and output voltage.

For CCM at a minimum input, calculate the converter duty cycle with Equation (7):

\[ D = \frac{(V_O + V_F) \cdot N}{(V_O + V_F) \cdot N + V_{in(min)}} \]  

(7)

Where \( V_F \) is the secondary diode’s forward voltage, \( N \) is the transformer turn ratio, and \( V_{in(min)} \) is the minimum voltage on the bulk capacitor.

The MOSFET turn-on time is calculated with Equation (8):

\[ T_{on} = D \cdot T_s \]  

(8)

Where \( T_s \) is the frequency jitter’s dominant switching period, and \( \frac{1}{T_s} = f_s = 65kHz \).

The average value of the primary current can be calculated with Equation (9):

\[ I_{av} = \frac{P_{in}}{V_{in(min)}} \]  

(9)

The peak value of the primary current can be calculated with Equation (10):

\[ I_{peak} = \frac{I_{av}}{(1 - K_P^2) \cdot D} \]  

(10)

The ripple value of the primary current can be calculated with Equation (11):

\[ I_{ripple} = K_P \cdot I_{peak} \]  

(11)

The valley value of the primary current can be calculated with Equation (12):

\[ I_{valley} = (1 - K_P) \cdot I_{peak} \]  

(12)

\( L_m \) can be calculated with Equation (13):

\[ L_m = \frac{V_{in(min)} \cdot T_{on}}{I_{ripple}} \]  

(13)

Current-Sense Resistor

Figure 12 shows the peak current comparator logic and the subsequent waveform. When the sum of the sensing resistor voltage and the slope compensator reaches \( V_{\text{peak}} \), the comparator goes high to reset the RS flip-flop, and the MOSFET is turned off.
The TIMER capacitor determines the frequency jitter period. A 10µA current source charges the capacitor when the TIMER voltage reaches 3.2V, and another 10µA current source discharges the capacitor to 2.8V. This charging and discharging cycle is repeated.

Equation (2) describes the jitter period in theory. A smaller $f_{\text{jitter}}$ is more effective for EMI reduction. However, the measurement bandwidth requires $f_{\text{jitter}}$ to be large compared to the spectrum analyzer $R_{BW}$ for effective EMI reduction. $f_{\text{jitter}}$ should also be less than the control loop gain crossover frequency to avoid disturbing the output voltage regulation.

The TIMER capacitor must be selected carefully. A capacitor that is too large may cause the start-up to fail at full load because of the long, soft start-up duration, shown in Equation (3). However, a TIMER capacitor that is too small causes the timer period to decrease, which overloads the timer count capability and may cause logic problems. For most applications, an $f_{\text{jitter}}$ value between 200Hz and 400Hz is recommended.

Ramp Compensation

In peak current control, subharmonic oscillation occurs when $D$ is greater than 0.5 in CCM. The HF500-7 solves this problem with internal ramp compensation. Calculate $\alpha$ with Equation (17):

$$\alpha = \frac{D_{\text{max}} \cdot V_{\text{in(min)}} \cdot R_{\text{sense}} \cdot m_a}{V_{\text{in(min)}} \cdot L_m \cdot R_{\text{sense}} + m_a}$$

Where $m_a = 20\text{mV}/\mu\text{s}$ is the minimum internal slope value of the compensation ramp, and $D_{\text{max}}$ are the slew rates of the primary-side and equivalent secondary-side voltages sensed by the current-sensing resistor respectively. For stable operation, $\alpha$ must be less than 1.

Jitter Period

Frequency jitter is used as an effective method for reducing EMI by dissipating energy. The $n_h$ order harmonic noise bandwidth is $B_{Tn} = n \cdot (2 \cdot \Delta f + f_{\text{jitter}})$, where $\Delta f$ is the frequency jitter amplitude. If $B_{Tn}$ exceeds the resolution bandwidth ($R_{BW}$) of the spectrum analyzer (200Hz for noise frequency less than 150kHz, 9kHz for noise frequency between 150kHz and 30MHz), the spectrum analyzer receives less noise energy.
PCB Layout Guidelines

Efficient PCB layout is critical for stable operation, good EMI performance, and good thermal performance. For best results refer to Figure 13 and follow the guidelines below:

1. Minimize the power stage loop area for better EMI performance. This includes the input loop (C4 - T1 - U1 - R1A/R1B - C4), the auxiliary winding loop (T1 - D6 - R8 - C7 - T1), the output loop (T1 - D7 - C12 - T1, T1 – D8 - C11 - T1), and the RCD snubber loop (T1 - R6 - D5 - R7/C6 - T1).

2. Keep the input loop GND and the control circuit GND separate and only connect them at C4. Otherwise, the IC operation may be influenced by noise.

3. Place one ceramic capacitor close to the sensitive IC pin (such as those for FB, B/O, and VCC) to decouple noise effectively.

4. Place a larger source area around the IC to improve thermal performance, if needed.

Design Example

Table 1 shows a design example of the HF500-7 for power adapter applications.

<p>| | |</p>
<table>
<thead>
<tr>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>V</strong></td>
<td><strong>I</strong></td>
</tr>
<tr>
<td><strong>IN</strong></td>
<td>85 to 265VAC</td>
</tr>
<tr>
<td><strong>VOUT1/ VOUT2</strong></td>
<td>12V/5V</td>
</tr>
<tr>
<td><strong>IOUT1/ IOUT2</strong></td>
<td>0.3A/0.3A</td>
</tr>
</tbody>
</table>

Figure 13: Recommended PCB Layout
TYPICAL APPLICATION CIRCUITS

Figure 14: Example of a Typical Application

Connection Diagram

Winding Diagram

Figure 15: Transformer Structure
### Table 2: Winding Order

<table>
<thead>
<tr>
<th>Tape (T)</th>
<th>Winding</th>
<th>Start-End</th>
<th>Wire Size (Φ)</th>
<th>Turns (T)</th>
<th>Tube</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>N1</td>
<td>5 → NC Clockwise</td>
<td>0.15*2</td>
<td>22</td>
<td>None</td>
</tr>
<tr>
<td>1</td>
<td>N2</td>
<td>3 → 5 Clockwise</td>
<td>0.15*1</td>
<td>168</td>
<td>None</td>
</tr>
<tr>
<td>1</td>
<td>N3</td>
<td>6 → 10 Clockwise</td>
<td>0.32*1 TIW</td>
<td>12</td>
<td>None</td>
</tr>
<tr>
<td>1</td>
<td>N4</td>
<td>8 → 10 Anticlockwise</td>
<td>0.45*1 TIW</td>
<td>9</td>
<td>None</td>
</tr>
<tr>
<td>3</td>
<td>N5</td>
<td>2 → 1</td>
<td>0.12*1</td>
<td>27</td>
<td>None</td>
</tr>
<tr>
<td></td>
<td>N6</td>
<td>1 → NC Clockwise</td>
<td>0.12*1</td>
<td>27</td>
<td></td>
</tr>
</tbody>
</table>
FLOW CHART

Start

Internal High Voltage Current Source On

Vcc > 12V

Y

N

Vcc > 12V

Y

N

Vcc < 1.5V

Y

N

Continuous Fault Monitor

Monitor Vcc

Continuous Fault Monitor

Vcc Decrease to 5.3V

Y

N

Latch Off the Switching Pulse

Vcc < 3V

Y

N

Monitor VFB

Vcc > 24V

Y

N

Vcc > 1.1V

Y

N

Monitor VFB

UVLO, brown-out, OTP & OLP are auto restart; OVP on VCC, and latch off on TIMER are latch mode. To release from the latch condition, unplug from the main input.

Figure 16: Control Flow Chart
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